

14.10 M12 x 1.25 CLASS 9.8
85% PROOF PRE-LOAD
5cm THICK ALUMINUM SANDWICH
FIND N_{sf} , N_{sy} & N_{ss}
GIVEN 20 kN (PEAK) FLUCTUATING LOAD

ME 340
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PRE-LOAD

$$F_i = .85 S_p A_t = .85 (650 \text{ MPa}) (92.07 \text{ mm}^2) (1 \text{E-}6 \frac{\text{m}}{\text{mm}^2}) = 50.869 \text{ kN}$$

$$S_p (\text{TABLE 14-7}) = 650 \text{ MPa}$$

$$A_t (\text{TABLE 14-2}) = 92.07 \text{ mm}^2$$

BOLT & JOINT STIFFNESS

$$K_b = \frac{\pi d^2 E_b}{4l} = \frac{\pi (.012 \text{ m})^2 207 \text{ GPa}}{4 (.05 \text{ m})} = 4.6822 \times 10^8 \text{ N/m}$$

$$K_m = \frac{2\pi d^2 E_m}{l} = \frac{2\pi (.012 \text{ m})^2 71.7 \text{ GPa}}{(.05 \text{ m})} = 12.974 \times 10^8 \text{ N/m}$$

LOAD ON BOLT DUE TO 20 kN EXTERNAL LOAD

$$P_b = P \frac{K_b}{K_m + K_b} = \frac{20 \text{ kN} (4.6822)}{(4.6822 + 12.974)} = 5.307 \text{ kN}$$

TOTAL LOAD ON BOLT

$$F_b = P_b + F_i = 5.307 + 50.869 \text{ kN} = 56.173 \text{ kN}$$

FACTOR OF SAFETY IN YIELD, N_{sy}

$$N_{sy} = \frac{S_y}{\sigma_{\text{bolt, max}}} = \frac{S_y A_t}{F_b} = \frac{720 \text{ MPa} (92.07 \text{ mm}^2) (1 \text{E-}6 \frac{\text{m}}{\text{mm}^2})}{56.173 \text{ kN}} = 1.18$$

$$S_y (\text{TABLE 14-7}) = 720 \text{ MPa}$$

BOLT STRESSES

$$P_{\max} = 20 \text{ kN}$$

$$P_{\min} = 0$$

$$P_{\text{alt}} = \frac{P_{\max} - P_{\min}}{2} = 10 \text{ kN}$$

$$P_{\text{mean}} = \frac{P_{\min} + P_{\max}}{2} = 10 \text{ kN}$$

$$\sigma_{\min} = \frac{k_b}{k_b + k_m} P_{\min} + \frac{F_i}{A_t} = \frac{F_i}{A_t} = \frac{50.869 \text{ kN}}{(92.07 \text{ mm}^2)(1 \text{E-}6 \text{ m}^2/\text{mm}^2)} = 553 \text{ MPa}$$

$$\sigma_{\max} = \frac{k_b}{k_b + k_m} P_{\max} + \frac{F_i}{A_t} = \frac{F_b}{A_t} = \frac{56.173 \text{ kN}}{92.07 \text{ mm}^2 (1 \text{E-}6 \text{ m}^2/\text{mm}^2)} = 610 \text{ MPa}$$

$$\sigma_{\text{MEAN}} = \frac{k_b}{k_b + k_m} \frac{P_{\text{mean}}}{A_t} + \frac{F_i}{A_t} = \frac{.2652(10 \text{ kN}) + 50.869 \text{ kN}}{92.07 \text{ mm}^2 (1 \text{E-}6 \text{ m}^2/\text{mm}^2)} = 581 \text{ MPa}$$

$$\sigma_{\text{alt}} = \frac{k_b}{k_b + k_m} \frac{P_{\text{alt}}}{A_t} = \frac{.2652(10 \text{ kN})}{92.07 \text{ mm}^2 (1 \text{E-}6 \text{ m}^2/\text{mm}^2)} = 28.8 \text{ MPa}$$

FACTOR OF SAFETY IN FATIGUE

$$N_{\text{SF}} = S_e \cdot \frac{S_{\text{ult}} - \sigma_{\min}}{[S_e \cdot (\sigma_{\text{MEAN}} - \sigma_{\min})] + S_{\text{ult}} \cdot \sigma_{\text{alt}}}$$

$$\begin{aligned} S_e &= .5 S_{\text{ult}} \cdot C_{\text{LOAD}} C_{\text{SIZE}} C_{\text{SURF}} \cdot \frac{1}{K_F} \\ &= .5(900 \text{ MPa})(.7)(.93)(.48) \frac{1}{3} \\ &= 46.9 \text{ MPa} \end{aligned}$$

$$N_{\text{SF}} = 46.9 \frac{900 - 553}{46.9(581 - 553) + 900 \cdot 28.8} = 0.60 \text{ (JOINT FAILS IN FATIGUE)}$$

FACTOR OF SAFETY IN JOINT SEPARATION

$F_m = 0$; FIND P_o SUCH THAT $F_m = 0$

$$N_{\text{sep}} = \frac{P_o}{P} = \frac{F_i(k_b + k_m)}{k_m} \cdot \frac{1}{P} = \frac{50.869 \text{ kN}(4.6822 + 12.974)}{12.974} \cdot \frac{1}{20 \text{ kN}} = 3.46$$

NOTES: FOS ARE DIFFERENT FROM TEXT DUE TO EFFECTIVE CYLINDER METHOD.