Statement:

A differential stress element has a set of applied stresses on it as indicated in each row of Table P4-1. For the row(s) assigned, draw the stress element showing the applied stresses, find the principal stresses and maximum shear stress analytically and check the results by drawing Mohr's circles for that stress state.

Solution:

See Table 4-1 for solution data to all rows of the problem statement. Only the variable sheet for row j is shown here. Also see the TKSolver file P04-01 which contains solutions for all rows. You may also run the program MOHR.EXE from the DOS partition of the CD-ROM supplied with the text and input the given data to see the Mohr's circles for any of the subsets (rows) of this problem.

| Table 4 | -1         | Results for all rows of Problem 4-1 |       |                 |                 |                 |  |  |  |  |
|---------|------------|-------------------------------------|-------|-----------------|-----------------|-----------------|--|--|--|--|
| Row     | $\sigma_1$ | σ <sub>2</sub>                      | σ3    | τ <sub>12</sub> | τ <sub>23</sub> | τ <sub>13</sub> |  |  |  |  |
| a       | 1207       | 0                                   | -207  | 604             | 104             | 707             |  |  |  |  |
| b       | 401        | 0                                   | -1401 | 201             | 701             | 901             |  |  |  |  |
| С       | 1118       | 0                                   | -1118 | 559             | 559             | 1118            |  |  |  |  |
| đ       | 311        | 0                                   | -1811 | 155             | 905             | 1061            |  |  |  |  |
| e       | 1059       | 0                                   | -59   | 530             | 30              | 559             |  |  |  |  |
| f       | 1311       | 0                                   | -811  | 655             | 405             | 1061            |  |  |  |  |
| g       | 1035       | 0                                   | -785  | 518             | 393             | 910             |  |  |  |  |
| h       | 1140       | 250                                 | 110   | 445             | 70              | 515             |  |  |  |  |
| i       | 1383       | -189                                | -1194 | 786             | 502             | 1289            |  |  |  |  |
| j       | 1127       | 568                                 | -1195 | 279             | 882             | 1161            |  |  |  |  |

## PROBLEM 4-3

Statement:

For the bicycle pedal-arm assembly in Figure P4-1 with a rider-applied force of 1500 N at the pedal, determine the maximum principal stress in the pedal arm if its cross section is 15 mm in dia. The pedal attaches to the pedal arm with a 12-mm screw thread. What is the stress in the pedal screw?

#### Solution:

Also see the TKSolver file P04-03.

| 770 | MPa | Max bending stress in pedal arm        |
|-----|-----|--|
| 531 | MPa | Max bending stress in pedal screw      |
| 136 | MPa | Max torsional shear stress in pedal ar |
| 793 | MPa | Max principal stress in pedal arm      |
| 0   | MPa | principal stress in pedal arm          |
| -23 | MPa | principal stress in pedal arm          |
| 408 | MPa | principal shear stress in pedal arm    |
| 396 | MPa | principal shear stress in pedal arm    |
| 12  | MPa | principal shear stress in pedal arm    |
|     |     |  |

## PROBLEM 4-4

Statement:

The trailer hitch shown in Figure P4-2 and Figure 1-1 (p. 12) has loads applied as defined in Problem 3-4. The tongue weight of 100 kg acts downward and the pull force of 4 905 N acts horizontally. Using the dimensions of the ball bracket shown in Figure 1-5 (p. 15 of text), determine:

- 114 M  $\rho_{\alpha}$  -(a) The principal stresses in the shank of the ball where it joins the ball bracket.
- 10 M  $\rho_{\tilde{a}}$  —(b) The bearing stress in the ball bracket hole.
- 7 M/A -(c) The tearout stress in the ball bracket.
  54 M/A -(d) The normal and shear stresses in the 19-mm dia attachment bolts,
  72 M/D -(e) The principal stresses in the ball bracket as a cantilever.

73 MPa Assumptions:

The nuts are only snug-tiaght (no preload) which is the worst case. All reactions are considered to be concentrated forces.

Statement:

A beam is supported and loaded as shown in Figure P4-11a Find the reactions, maximum shear, maximum moment, maximum slope, maximum bending stress, and maximum deflection for the data given in

the assigned row(s) in Table P4-2.

Solution:

See Table 4-23 for solution data to all rows of the problem statement. Only the variable sheet for row a is shown here. Also see the TKSolver

file P04-23 which contains solutions for all rows.

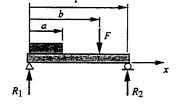


FIGURE 4-23A

Free Body Diagram for Problem 4-23

| param<br>units | R I<br>N | R 2<br>N | Vmin<br>N | Vmax<br>N | Mmin<br>N-m | Mmax<br>N-m | tmin<br>deg | tmax<br>deg | ymin<br>mm | ymax<br>mm | stress<br>MPa |
|----------------|----------|----------|-----------|-----------|-------------|-------------|-------------|-------------|------------|------------|---------------|
| Row            |          |          |           | • • •     |             |             |             |             |            |            |               |
| a              | 264      | 316      | -316      | 264       | 0.0         | 126         | -0.31       | 0.33        | -1.82      | 0.00       | 88.7          |
| b              | 378      | 488      | -488      | 378       | 0.0         | 146         | -0.40       | 0.44        | -1.69      | 0.00       | 85.9          |
| c              | 192      | 308      | -308      | . 192     | 0.0         | 31          | -0.13       | 0.15        | -0.24      | 0.00       | 81.2          |
| d              | 85       | 198      | -198      | 85        | 0.0         | 40          | -0.41       | 0.54        | -2.07      | 0.00       | 88.7          |
| e              | 336      | 448      | -448      | 336       | 0.0         | 156         | -0.49       | 0.55        | -2.53      | 0.00       | 78.1          |
| f              | 256      | 775      | -775      | 256       | 0.0         | 77          | -0.20       | 0.28        | -0.63      | 0.00       | 66.2          |
| g              | 95       | 225      | -225      | 95        | 0.0         | 22          | -0.31       | 0.41        | -1.11      | 0.00       | 52.5          |
| h              | 205      | 335      | -335      | 205       | 0.0         | 23          | -0.22       | 0.26        | -0.27      | 0.00       | 29.3          |
| i              | 56       | 151      | -151      | 56        | 0.0         | 15          | -0.38       | 0.52        | -0.98      | 0.00       | 27.5          |
| j              | 31       | 64       | -64       | 31        | 0.0         | 3           | -0.19       | 0.24        | -0.23      | 0.00       | 27.0          |
| k              | 229      | 662      | -662      | 229       | 0.0         | 66          | -0.10       | 0.15        | -0.27      | 0.00       | 22.3          |
| 1              | 86       | 536      | -536      | 86        | 0.0         | 53          | -0.18       | 0.30        | -1.07      | 0.00       | 9.5           |
| m              | 79       | 429      | -429      | 79        | 0.0         | 43          | -0.22       | 0.36        | -1.03      | 0.00       | 13.2          |
| ח              | 29       | 100      | -100      | 29        | 0.0         | 15          | -0.27       | 0.40        | -1.47      | 0.00       | 18.8          |

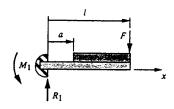
## PROBLEM 4-24

**Statement**:

A beam is supported and loaded as shown in Figure P4-11b, find the reactions, the maximum shear, maximum moment, maximum slope, maximum bending stress, and maximum deflection for the data given in the assigned row(s) in Table P4-2.

Solution:

See Table 4-24 for solution data to all rows of the problem statement. Only the variable sheet for row a is shown here. Also see the *TKS* olver file P04-24 which contains solutions for all rows.



# FIGURE 4-24A

Free Body Diagram for Problem 4-24

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Statement:

For the bracket shown in Figure P4-14 and the data in the row(s) assigned from Table P4-3, determine the bending stress at point A and the shear stress due to transverse loading at point B. Also find the torsional shear stress at both points. Then determine the principal stresses at points A and B.

Solution:

See Table 4-33 for solution data to all rows of the problem statement. Only the variable sheet for row a is shown here. Also see the TKSolver file P04-33 which contains solutions for all rows.

| Table 4-33 Summary of results for all rows of Problem 4-33 |                 |                      |                      |                 |                 |                 |                     |                 |                 |                 |                    |
|--|-----------------|----------------------|----------------------|-----------------|-----------------|-----------------|---------------------|-----------------|-----------------|-----------------|--------------------|
| param<br>units   | σx<br>@A<br>MPa | τ bend<br>@ A<br>MPa | τ tors<br>@ A<br>MPa | σ1<br>@A<br>MPa | σ2<br>@A<br>MPa | σ3<br>@A<br>MPa | τ max<br>@ A<br>MPa | σ1<br>@B<br>MPa | σ2<br>@B<br>MPa | σ3<br>@B<br>MPa | τ max<br>@B<br>MPa |
| Row  |                 |                      |                      |                 |                 |                 |                     |                 |                 |                 |                    |
| а  | 8               | 0.6                  | 16.8                 | 21.5            | 0               | -13.1           | 17                  | 16.1            | 0               | -16.1           | 16.1               |
| b  | 8               | 0.6                  | 10.9                 | 15.4            | 0               | -7.7            | 12                  | 10.3            | 0               | -10.3           | 10.3               |
| С  | 24              | 0.7                  | 3.9                  | 24.3            | 0               | -0.6            | 12                  | 3.2             | 0               | -3.2            | 3.2                |
| d  | 14              | 0.2                  | 4.4                  | 15.4            | 0               | -1.3            | 8                   | 4.2             | 0               | -4.2            | 4.2                |
| e  | 5               | 0.9                  | 10                   | 12.7            | 0               | -7.9            | 10                  | 9.1             | 0               | -9.1            | 9.1                |
| f  | 4               | 1.5                  | 8                    | 10.5            | 0               | -6.1            | 8                   | 6.5             | 0               | -6.5            | 6.5                |
| g  | 16              | 1.3                  | 13.7                 | 23.7            | 0               | -8              | 16                  | 12.4            | 0               | -12.4           | 12.4               |
| h  | 29              | 2                    | 7.3                  | 31              | 0               | -1.7            | 16                  | 5.3             | 0               | -5.3            | 5.3                |
| i  | 16              | 0.8                  | 3                    | 16.3            | 0               | -0.5            | 8                   | 2.1             | 0               | -2.1            | 2.1                |
| j  | 18              | 1.5                  | 4.5                  | 19.1            | 0               | -1.1            | 10                  | 3               | 0               | -3              | 3                  |
| k  | 8               | 1.6                  | 6                    | 11.2            | 0               | -3.2            | 7                   | 4.4             | 0               | -4.4            | 4.4                |
| 1  | 9               | 1                    | 7.4                  | 13.1            | 0               | -4.2            | 9                   | 6.4             | 0               | -6.4            | 6.4                |
| m  | 15              | 3.2                  | 10.5                 | 20.2            | 0               | -5.5            | 13                  | 7.3             | 0               | -7.3            | 7.3                |
| n  | 11              | 1.5                  | 10                   | 17.1            | 0               | -5.8            | 11                  | 8.5             | 0               | -8.5            | 8.5                |

## PROBLEM 4-34

Statement:

For the bracket shown in Figure P4-14 and the data in the row(s) assigned from Table P4-3, determine the deflection at load F.

Solution:

See Table 4-34 for solution data to all rows of the problem statement. Only the variable sheet for row a is shown here. Also see the TKSolver file P04-34 which contains solutions for all rows.

# PROBLEM 4-35

Statement:

For the bracket shown in Figure P4-14 and the data in the row(s) assigned from Table P4-3, determine the spring rate of the tube in bending, the spring rate of the arm in bending and the spring rate of the tube in torsion. Combine these into an overall spring rate in terms of the force F and the linear deflection at force F.

Solution:

See Table 4-35 for solution data to all rows of the problem statement. Only the variable sheet for row a is shown here. Also see the *TKS* olver file P04-35 which contains solutions for all rows.

| Table 4-34 | Deflection for all |
|------------|--------------------|
|            | rows of Prob. 4-34 |

|     | y                      |
|-----|------------------------|
| Row | $\mathbf{m}\mathbf{m}$ |
|     |                        |
| a   | -1.62                  |
| ь   | -0.20                  |
| c   | -0.39                  |
| d   | -5.43                  |
| e   | -0.91                  |
| f   | -0.97                  |
| g   | -4.98                  |
| h   | -7.91                  |
| i   | -0.36                  |
| j   | -11.57                 |
| k   | -0.46                  |
| 1 . | -0.55                  |
| m   | -0.06                  |
| n   | -0.12                  |

Table 4-35 Results for all rows of Problem 4-35

|     | K    |
|-----|------|
| Row | N/mm |
|     |      |
| a   | 31   |
| b   | 427  |
| С   | 241  |
| đ   | 29.5 |
| е   | 994  |
| f   | 982  |
| g   | 171  |
| h   | 101  |
| i   | 2658 |
| j   | 51.9 |
| k   | 1906 |
| I   | 1357 |
| m   | 8290 |
| n   | 6795 |
|     |      |

Statement:

For the bracket shown in Figure P4-14 and the data in the row(s) assigned from Table P4-3, redo Problem 4-33 considering the stress concentration at points A and B. Assume a stress-concentration factor of 2.5 in both bending and torsion.

Solution:

See Table 4-36 for solution data to all rows of the problem statement. Only the variable sheet for row a is shown here. Also see the TKSolver file P04-36 which contains solutions for all rows.

| param | σx         | τ bend     | τtors      | σ1         | σ2         | σ3         | τmax       | σ1        | σ2        | σ3        | τmax      |
|-------|------------|------------|------------|------------|------------|------------|------------|-----------|-----------|-----------|-----------|
|       | @ A<br>MPa | @B<br>MPa | @B<br>MPa | @B<br>MPa | @B<br>MPa |
| Row   |            |            |            |            |            |            |            |           |           |           | WII a     |
| a     | 8.40       | 0.60       | 16.8       | 21.5       | 0          | -13.1      | 17         | 16.1      | 0         | -16.1     | 16.0      |
| ь     | 7.60       | 0.60       | 10.9       | 15.4       | 0          | -7.7       | 12         | 10.3      | 0         | -10.3     | 10.0      |
| С     | 23.60      | 0.70       | 3.9        | 24.3       | 0          | -0.6       | 12         | 3.2       | 0         | -3.2      | 3.0       |
| ď     | 14.10      | 0.20       | 4.4        | 15.4       | 0          | -1.3       | 8          | 4.2       | 0         | -4.2      | 4.0       |
| e     | 4.90       | 0.90       | 10         | 12.7       | 0          | -7.9       | 10         | 9.1       | 0         | -9.1      | 9.0       |
| f     | 4.40       | 1.50       | 8          | 10.5       | 0          | -6.1       | 8          | 6.5       | 0         | -6.5      | 6.0       |
| g     | 15.70      | 1.30       | 13.7       | 23.7       | 0          | -8         | 16         | 12.4      | 0         | -12.4     | 12.0      |
| h     | 29.30      | 2.00       | 7.3        | 31         | 0          | -1.7       | 16         | 5.3       | 0         | -5.3      | 5.0       |
| i     | 15.70      | 0.80       | 3          | 16.3       | 0          | ~0.5       | 8          | 2.1       | 0         | -2.1      | 2.0       |
| j     | 18.00      | 1.50       | 4.5        | 19.1       | 0          | -1.1       | 10         | 3         | 0         | -3        | 3.0       |
| k     | 8.00       | 1.60       | 6          | 11.2       | 0          | -3.2       | 7          | 4.4       | 0         | -4.4      | 4.0       |
| 1     | 8.90       | 1.00       | 7.4        | 13.1       | 0          | -4.2       | 9          | 6.4       | 0         | -6.4      | 6.0       |
| m     | 14.80      | 3.20       | 10.5       | 20.2       | 0          | -5.5       | 13         | 7.3       | 0         | -7.3      | 7.0       |
| n     | 11.30      | 1.50       | 10         | 17.1       | 0          | -5.8       | 11         | 8.5       | 0         | -8.5      | 8.0       |