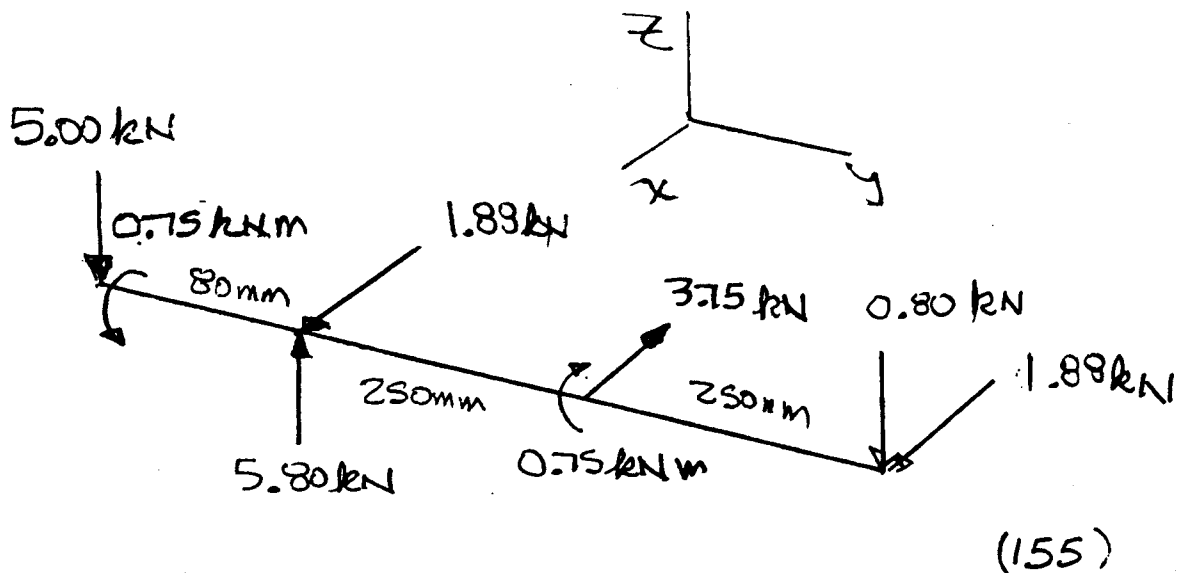


NAME: _____

8:00 AM

- Read all problems carefully. Check the board for any additions or corrections.
 - Show all work, which must be neat and orderly to be graded. That is, sloppy work will not be graded!
 - Show no work on this page. Return this page with your solutions.
- (1) A sliding element bearing has a length of 2.50 inches, a diameter of 1.25 inches, and a load of 400 pounds, corresponding to a rotational speed of 1150 rev/minute. The lubricant is SAE 40 with a viscosity of $10 \mu\text{reyn}$. Determine the temperature rise across the bearing, supply and outlet oil temperatures, coefficient of friction, eccentricity, total and side oil flows, maximum oil pressure, and the power lost in the bearing. Use a radial clearance 0.001 inches.
 - (2) For the design of problem (1) select a 300 series rolling element bearing which has a reliability of 95% and must last for 20,000 hours. The application is one with moderate impact.
 - (3) For the figure shown below, verify the free body diagram is correct.
 - (4) A bearing has been operated at 2,500,000 cycles at 25,000-N. Can this bearing be operated at 15,000-N for an additional 250,000 cycles? The bearing is an 02 series with a bore diameter of 60-mm.



① $\left. \begin{array}{l} l = 2.5 \text{ in} \\ d = 1.25 \text{ in} \\ \frac{l}{d} = 2 \\ W = 400 \text{ lb} \end{array} \right\} \rightarrow P = \frac{W}{ld} = \frac{400 \text{ lb}}{(2.5)(1.25) \text{ in}^2} = 128 \text{ psi}$

$c = 0.001 \text{ in}$

$\frac{r}{c} = \frac{0.625}{0.001} = 625$

$N = 1150 \frac{\text{rev}}{\text{min}} \times \frac{1 \text{ min}}{60 \text{ sec}} = 19.2 \text{ rev/sec}$

SAE 40

$T_{\text{AVG}} @ 10 \mu \text{ reyn} = 122^\circ \text{F}$

FIRST, THE SOMMERFELD NUMBER:

$$S = \left(\frac{r}{c}\right)^2 \left(\frac{\mu N}{P}\right) = (625)^2 \left(\frac{10 \times 10^{-6} \text{ reyn} (19.2 \frac{\text{rev}}{\text{sec}})}{128 \text{ psi}}\right) = 0.59$$

NOW THE TEMP RISE:

$$\Delta T_F = \frac{0.103 P}{1 - 0.5 \frac{Q_s}{Q}} \frac{\frac{f}{c} P}{\frac{Q}{r c N l}} = \frac{0.103 (128)}{1 - 0.5 (0.15)} \frac{10}{3.5} = 41^\circ \text{F}$$

IN & OUT TEMPS:

$T_{\text{AVG}} = 122^\circ \text{F} \quad T_i = T_{\text{AVG}} - \frac{1}{2} \Delta T = 122 - 20.5 = 121.5^\circ \text{F}$

$T_o = T_{\text{AVG}} + \frac{1}{2} \Delta T = 122 + 20.5 = 142.5^\circ \text{F}$

COEFFICIENT OF FRICTION:

$\frac{f}{c} = 10 ; f = \frac{10}{625} = 0.016$

ECCENTRICITY:

$\Sigma = 0.12 = e/c \rightarrow e = 0.12 (0.001) = 0.00012 \text{ in}$

① CONT'D

TOTAL & SIDE FLOWS:

$$\frac{Q}{rcNl} = 3.5 \rightarrow Q = 3.5(-.625 \text{ in})(0.001 \text{ in})(19.2 \frac{\text{rev}}{\text{sec}})(2.5 \text{ in}) \\ = 0.105 \text{ in}^3/\text{sec}$$

$$\frac{Q_s}{Q} = 0.15 \rightarrow Q_s = 0.15(0.105 \text{ in}^3/\text{sec}) = 0.016 \text{ in}^3/\text{sec}$$

MAX OIL PRESSURE:

$$\frac{P}{P_{\max}} = 0.65 \rightarrow P_{\max} = \frac{128 \text{ psi}}{0.65} = 197 \text{ psi}$$

POWER LOST:

$$H_p = \frac{F_w r N}{10550} = \frac{0.016(400 \text{ lb})0.625 \text{ in}(19.2 \frac{\text{rev}}{\text{sec}})}{10550} = 0.073 \text{ hp}$$

②

300 series brg.

reliab = 95% $\rightarrow k_R = 0.62$

$$20,000 \text{ hrs} \times 1150 \frac{\text{rev}}{\text{min}} \times 60 \frac{\text{min}}{\text{hr}} = 1.38 \text{ E}9 \text{ cycles}$$

MODERATE IMPACT $\rightarrow k_a = 1.75$ (1.5-2.0)

$$C_{\text{REQ}} = k_a F_e \left(\frac{L}{k_R L_R} \right)^{0.3} = 1.75(400 \text{ lb}) \left(\frac{1.38 \text{ E}9}{.62(90 \text{ E}6)} \right)^{0.3} = 1,833 \text{ lb} \\ = 8.2 \text{ kN}$$

CHOOSE 30mm BORE RADIAL BALL \rightarrow 306 OR LARGER

OR 30mm BORE ANGULAR CONTACT \rightarrow 306 OR LARGER

SHAFT CS 1.25in \rightarrow 31.75mm dia. \rightarrow 307 BRG

③ $\sum F_x = 1.88 \text{ kN} - 3.75 \text{ kN} + 1.88 \text{ kN} = 0$
 $\sum F_y = 0$
 $\sum F_z = -5.00 \text{ kN} + 5.80 \text{ kN} - 0.80 \text{ kN} = 0$
 $\sum M_x = 5.80 \text{ kN}(80 \text{ mm}) - 0.80 \text{ kN}(580 \text{ mm}) = 0$
 $\sum M_y = 0.75 \text{ kNm} - 0.75 \text{ kNm} = 0$
 $\sum M_z = -1.88 \text{ kN}(80 \text{ mm}) + 3.75 \text{ kN}(330 \text{ mm}) - 1.88 \text{ kN}(580 \text{ mm}) = 0$
 LOOKS LIKE IT'S IN EQUILLIBRIUM TO ME.

④ $\frac{l_1}{L_1} + \frac{l_2}{L_2} \leq 1 \rightarrow l_2 \leq \left(1 - \frac{l_1}{L_1}\right) L_2$
 $l_1 = 2.5 \text{ EG}$
 $l_2 = .25 \text{ EG}$
 $L_1 = 1 \text{ EG} \left(\frac{47.5}{25}\right)^{3.33} = 8.5 \text{ EG}$
 $L_1 = 1 \text{ EG} \left(\frac{47.5}{15}\right)^{3.33} = 46 \text{ EG}$
 $l_2 \leq 32 \text{ EG} \checkmark$
 LOADING O.K.

DEEP GROOVE
 $C = 47.5 \text{ kN}$

$L_1 = 1 \text{ EG} \left(\frac{55.9}{25}\right)^{3.33} = 1.5 \text{ EG}$
 $L_2 = 1 \text{ EG} \left(\frac{55.9}{15}\right)^{3.33} = 80 \text{ EG}$
 $l_2 \leq 67 \text{ EG} \checkmark$
 LOADING O.K.

ANGULAR CONTACT
 $C = 55.9 \text{ kN}$