

## BRAKES ~ EXAMPLE PROBLEM

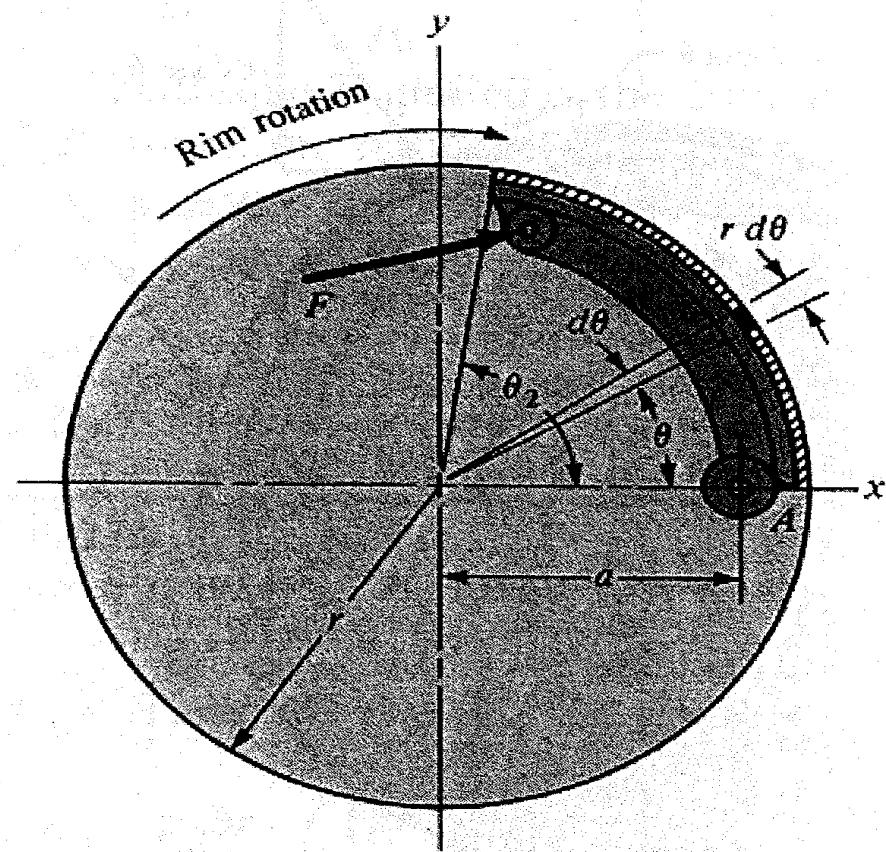
Reference: Shigley, 5<sup>th</sup> Edition

### Problem 16.4

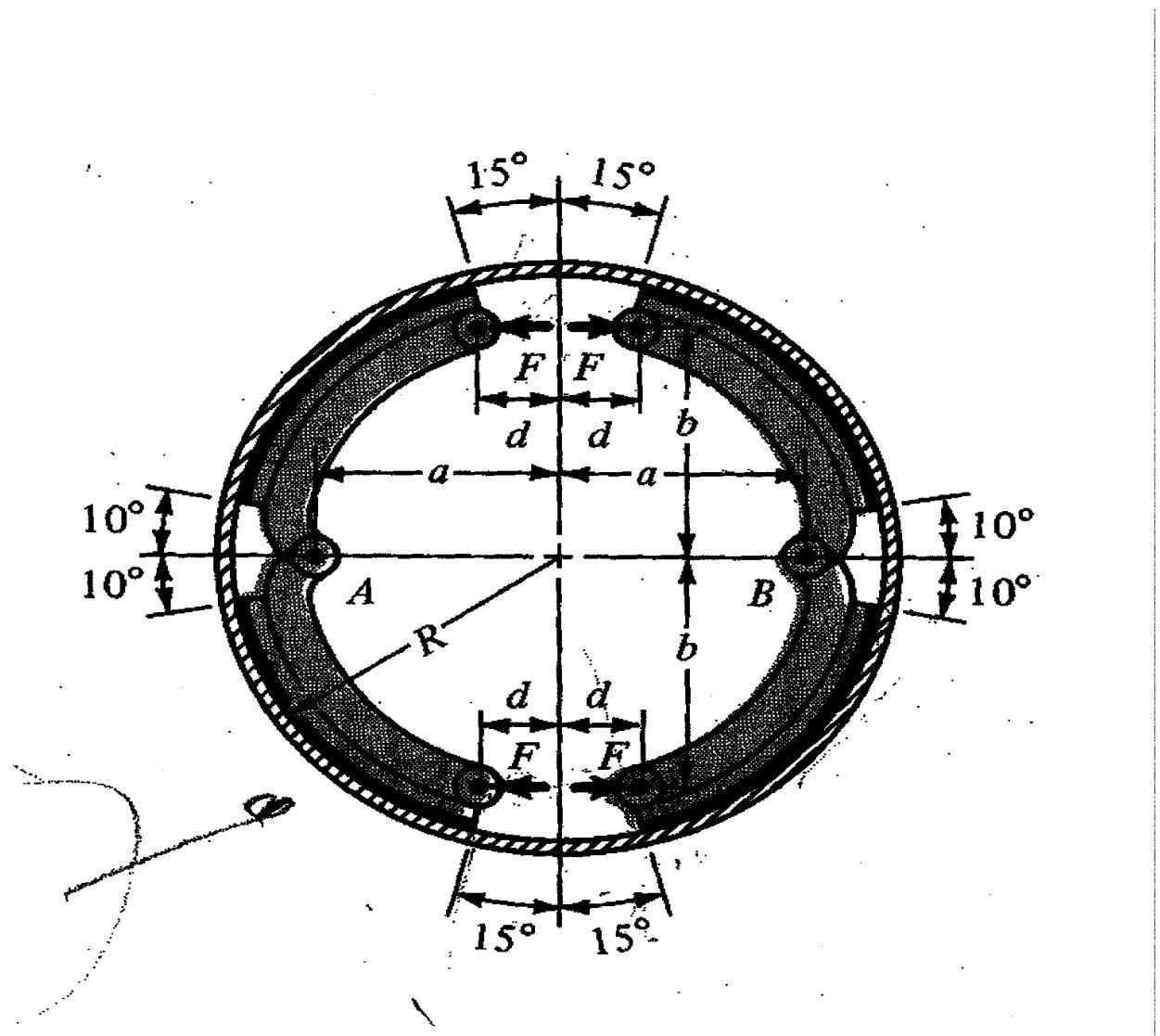
The figure below shows a 400-mm diameter brake drum with four (4) internally expanding shoes. Each of the hinge pins A and B supports a pair of shoes. The actuating mechanism is to be arranged to produce the same force  $F$  on each shoe. The face width of the shoes is 75-mm. The material used has a coefficient of friction of 0.24 and a maximum pressure of 1-mPa. Determine:

- (a) Actuating force
- (b) Braking capacity
- (c) Noting the rotation may be in either direction, compute the hinge-pin reactions.

$$P_\Theta = P_a \frac{\sin \theta}{\sin \theta_a}$$



**Internal Friction Shoe**



Dimensions are in millimeters and are:

$$a = 150$$

$$b = 165$$

$$d = 50$$

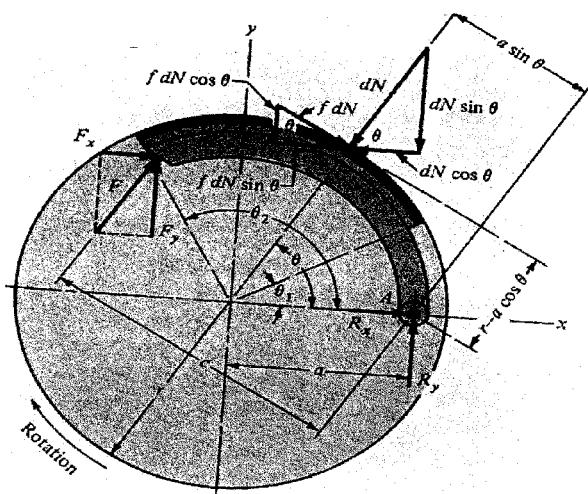
$p$  = unit pressure acting upon an element of area of the frictional material located at an angle  $\theta$  from the hinge pin.

$p_a$  = maximum pressure located at an angle  $\theta_a$  from the hinge pin.

$p = \max @ \theta = 90\text{-degrees}$ .

If the ***toe angle***,  $\theta_2$ , is less than 90-degrees, maximum pressure will occur at the toe.

When  $\theta = 0$ ,  $p = 0$ ; material at the toe contributes little to the friction force.



Brake Shoe Forces

$$M_s = \frac{\rho_p br}{\sin \theta_a} \int_{\theta_1}^{\theta_2} \sin(\theta)(r - a \cos \theta) d\theta$$

= moment of Frictional Forces  
about pin.

$$M_N = \frac{\rho p br}{\sin \theta_a} \int_{\theta_1}^{\theta_2} \sin^2 \theta d\theta$$

= moment of normal forces  
about pin

$$F = \frac{M_N - M_s}{c}$$

- Actuating Force

$$M_N = M_s$$

- Self-locking

$\alpha$  must be s.t.  $M_N > M_s$  - for  
Self-energizing.

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Above derived from:

$$M_g = \int f_N (r - a \cos \theta) d\theta$$

$$M_H = \int dN (a \sin \theta) d\theta$$

Torque applied by shoe:

$$T = \int f_r dN = \frac{p_a b r^2}{\sin \theta_a} \int_{\theta_1}^{\theta_2} \sin \theta d\theta$$

$$T = \frac{p_a b r^2 (\cos \theta_1 - \cos \theta_2)}{\sin \theta_a}$$

Pin reactions:

$$\begin{aligned} R_x &= \int dN \cos \theta - \int f_h \sin \theta - F_x \\ &= \frac{p_a b r}{\sin \theta_a} \left( \int_{\theta_1}^{\theta_2} \sin \theta \cos \theta d\theta \right. \\ &\quad \left. - \int_{\theta_1}^{\theta_2} \sin^2 \theta d\theta \right) - F_x \end{aligned}$$

Similarly:

$$\begin{aligned} R_y &= \frac{p_a b r}{\sin \theta_a} \int_{\theta_1}^{\theta_2} \sin^2 \theta d\theta + \int_{\theta_1}^{\theta_2} \sin \theta \cos \theta d\theta \\ &\quad - F_y \end{aligned}$$

IF direction reversed

$$F = \frac{M_H + M_g}{c}$$

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$$A = \int_{\theta_1}^{\theta_2} \sin \theta \cos \theta d\theta = \frac{1}{2} \sin^2 \theta \Big|_{\theta_1}^{\theta_2}$$

$$B = \int_{\theta_1}^{\theta_2} \sin^2 \theta d\theta = \left[ \frac{\theta}{2} - \frac{\sin 2\theta}{4} \right] \Big|_{\theta_1}^{\theta_2}$$

$$\therefore R_x = \frac{-p_a br}{\sin \theta_a} (A - \frac{1}{2}B) - F_x$$

$$R_y = \frac{-p_a br}{\sin \theta_a} (B + \frac{1}{2}A) - F_y$$

$$= R_x = \frac{-p_a br}{\sin \theta_a} (A + \frac{1}{2}B) - F_x$$

$$R_y = \frac{-p_a br}{\sin \theta_a} (B - \frac{1}{2}A) - F_y$$

Reference system ~ origin at center  
drum.

- Positive x-axis, thru hinge pin
- Positive y-axis, in direction of shoe.

Problem:

$$\theta_1 = 10^\circ$$

$$\theta_2 = 75^\circ$$

$$\therefore \theta_a = 75^\circ$$

Let  $\alpha = [r \int_{\theta_1}^{\theta_2} \sin \theta d\theta - a \int_{\theta_1}^{\theta_2} \sin \theta \omega \theta d\theta]$

①  $\alpha = [r \int_{\theta_1}^{\theta_2} \sin \theta d\theta - a A]$

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$$\textcircled{3} \quad S = \int_{0}^{\theta_a} \sin^2 \theta d\theta = \left[ \frac{\theta}{2} - \frac{\sin 2\theta}{4} \right]_{10}^{75}$$

$$= B$$

$$A = \int_{0}^{\theta_a} \sin \theta \cos \theta d\theta = \frac{1}{2} \sin^2 \theta \Big|_{10}^{75}$$

$$\cancel{\frac{1}{2} \sin^2 \theta} \Big|_{10}^{75}$$

$$A = 0.951$$

$$B = 0.527$$

$$\alpha = r [-\cos \theta] \Big|_{10}^{75} - \alpha A$$

$$r = 200 \text{ mm}$$

$$\alpha = 150 \text{ mm}$$

$$\alpha = 77.5 \text{ mm}$$

$$\alpha$$

$$M_S = \left( \frac{S_p b r}{\sin \theta_a} \right) \alpha \cancel{-} \frac{N}{m} \\ = \frac{(0.24)[1 \times 10^6](0.075 \text{ m})(0.200 \text{ m})}{\sin(75)} (0.08) \text{ m} \quad [0.075 \text{ m}]$$

$$M_f = 290 \text{ N.m}$$

$$M_N = \frac{P_a b r a}{\sin \theta_a} B$$

$$M_N = \frac{(1 \times 10^6 \frac{N}{m^2})(0.075 \text{ m})(0.2 \text{ m})(-0.15 \text{ m})}{\sin(75)} (0.53)$$

$$M_N = 1230 \text{ N.m}$$

National Brand  
13-720 500 SHEETS FELT 5 SQUARE  
42-361 50 SHEETS EYELET 5 SQUARE  
100 SHEETS EYELET 5 SQUARE  
42-352 200 RECYCLED WHITE 5 SQUARE  
42-353 100 RECYCLED WHITE 5 SQUARE  
42-359 200 RECYCLED WHITE 5 SQUARE  
Made in U.S.A.

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$$F = \frac{M_N - M_S}{c}$$
$$= \frac{1230 - 289}{0.165} \text{ N.m}$$

$$F = \begin{cases} 5.7 \text{ KN.m} \\ 5700 \text{ N.m} \end{cases}$$

For the primary shoe:

$$T = \frac{S_p a b r^2 (\cos \theta_1 - \cos \theta_2)}{\sin \theta_a}$$

$$T = \frac{(0.15m)(1 \times 10^6 \frac{N}{m^2})(\cos 75 - \cos 10)(0.24)(0.2)^2 m^2}{\sin 75}$$

$$T = 541 \text{ N.m}$$

For the secondary shoe:

$$F = \frac{M_N + M_S}{c} = 5700 \text{ N}$$

$$(F_{\text{primary}} = F_{\text{secondary}})$$

$$M_N = \frac{1230}{10^6} \text{ Pa}$$

$$M_S = \frac{289}{10^6} \text{ Pa}$$

$$5700 = \left(\frac{1230}{10^6}\right) p_a + \left(\frac{289}{10^6}\right) p_a$$
$$\cdot 165$$

$$p_a = 0.62 \times 10^6 \text{ Pa}$$

$$T = 335 \text{ N.m}$$

$$\begin{aligned} T_{\text{TOTAL}} &= T_L + T_R \\ &= (2)(521) + (2)(335) \end{aligned}$$

$$T_{\text{TOTAL}} = 1750 \text{ N.m}$$

= Braking capacity

$$R_x = -0.65 \text{ kN}$$

$$R_y = 3.87 \text{ kN}$$

Primary

$$R_x = -0.14 \text{ kN}$$

$$R_y = 4.02 \text{ kN}$$

Secondary