

# Solutions to Even numbered problems in Chapters 5-7

## CHAPTER 5 (Sections 5.1-5.8)

- 5-2. 1) The parameter of interest is the difference in breaking strengths,  $\mu_1 - \mu_2$  and  $\Delta_0 = 10$   
 2)  $H_0 : \mu_1 - \mu_2 = 10$  or  $\mu_1 = \mu_2$   
 3)  $H_1 : \mu_1 - \mu_2 > 10$  or  $\mu_1 > \mu_2$   
 4)  $\alpha = 0.05$   
 5) The test statistic is

$$z_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{\sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}}$$

- 6) Reject  $H_0$  if  $z_0 > z_{\alpha} = 1.645$   
 7)  $\bar{x}_1 = 162.5$   $\bar{x}_2 = 155.0$   $\delta = 10$   
 $\sigma_1 = 1.0$   $\sigma_2 = 1.0$   
 $n_1 = 10$   $n_2 = 12$

$$z_0 = \frac{(162.5 - 155.0) - 10}{\sqrt{\frac{(1.0)^2}{10} + \frac{(1.0)^2}{12}}} = -5.84$$

- 8) Since  $-5.84 < 1.645$  do not reject the null hypothesis and conclude there is insufficient evidence to support the use of plastic 1 at  $\alpha = 0.05$ .

- 5-4.  $\bar{x}_1 = 30.87$   $\bar{x}_2 = 30.68$   
 $\sigma_1 = 0.10$   $\sigma_2 = 0.15$   
 $n_1 = 12$   $n_2 = 10$

- a) 90% two-sided confidence interval:

$$(\bar{x}_1 - \bar{x}_2) - z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}} \leq \mu_1 - \mu_2 \leq (\bar{x}_1 - \bar{x}_2) + z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}$$

$$(30.87 - 30.68) - 1.645 \sqrt{\frac{(0.10)^2}{12} + \frac{(0.15)^2}{10}} \leq \mu_1 - \mu_2 \leq (30.87 - 30.68) + 1.645 \sqrt{\frac{(0.10)^2}{12} + \frac{(0.15)^2}{10}}$$

$$0.0987 \leq \mu_1 - \mu_2 \leq 0.2813$$

We are 90% confident that the mean fill volume for machine 1 exceeds that of machine 2 by between 0.0987 and 0.2813 fl. oz.

- b) 95% two-sided confidence interval:

$$(\bar{x}_1 - \bar{x}_2) - z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}} \leq \mu_1 - \mu_2 \leq (\bar{x}_1 - \bar{x}_2) + z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}$$

$$(30.87 - 30.68) - 1.96 \sqrt{\frac{(0.10)^2}{12} + \frac{(0.15)^2}{10}} \leq \mu_1 - \mu_2 \leq (30.87 - 30.68) + 1.96 \sqrt{\frac{(0.10)^2}{12} + \frac{(0.15)^2}{10}}$$

$$0.081 \leq \mu_1 - \mu_2 \leq 0.299$$

We are 95% confident that the mean fill volume for machine 1 exceeds that of machine 2 by between 0.081 and 0.299 fl. oz.

Comparison of parts a and b:

As the level of confidence increases, the interval width also increases (with all other values held constant).

c) 95% upper-sided confidence interval:

$$\mu_1 - \mu_2 \leq (\bar{x}_1 - \bar{x}_2) + z_{\alpha} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}$$

$$\mu_1 - \mu_2 \leq (30.87 - 30.68) + 1.645 \sqrt{\frac{(0.10)^2}{12} + \frac{(0.15)^2}{10}}$$

$$\mu_1 - \mu_2 \leq 0.2813$$

With 95% confidence, we believe the fill volume for machine 1 exceeds the fill volume of machine 2 by no more than 0.2813 fl. oz.

5-6.  $\bar{x}_1 = 89.6$   $\bar{x}_2 = 92.5$   
 $\sigma_1^2 = 1.5$   $\sigma_2^2 = 1.2$   
 $n_1 = 15$   $n_2 = 20$

a) 95% confidence interval:

$$(\bar{x}_1 - \bar{x}_2) - z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}} \leq \mu_1 - \mu_2 \leq (\bar{x}_1 - \bar{x}_2) + z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}$$

$$(89.6 - 92.5) - 1.96 \sqrt{\frac{1.5}{15} + \frac{1.2}{20}} \leq \mu_1 - \mu_2 \leq (89.6 - 92.5) + 1.96 \sqrt{\frac{1.5}{15} + \frac{1.2}{20}}$$

$$-3.684 \leq \mu_1 - \mu_2 \leq -2.116$$

With 95% confidence, we believe the mean road octane number for formulation 2 exceeds that of formulation 1 by between 2.116 and 3.684.

b) 1) The parameter of interest is the difference in mean road octane number,  $\mu_1 - \mu_2$  and  $\Delta_0 = 0$

2)  $H_0: \mu_1 - \mu_2 = 0$  or  $\mu_1 = \mu_2$

3)  $H_1: \mu_1 - \mu_2 < 0$  or  $\mu_1 < \mu_2$

4)  $\alpha = 0.05$

5) The test statistic is

$$z_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{\sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}}$$

6) Reject  $H_0$  if  $z_0 < -z_{\alpha} = -1.645$

7)  $\bar{x}_1 = 89.6$   $\bar{x}_2 = 92.5$

$\sigma_1^2 = 1.5$   $\sigma_2^2 = 1.2$

$n_1 = 15$   $n_2 = 20$

$$z_0 = \frac{(89.6 - 92.5) - 0}{\sqrt{\frac{(1.5)^2}{15} + \frac{(1.2)^2}{20}}} = -7.254$$

8) Since  $-7.25 < -1.645$  reject the null hypothesis and conclude the mean road octane number for formulation 2 exceeds that of formulation 1 using  $\alpha = 0.05$ .

c) P-value =  $P(z \leq -7.25) = 1 - P(z \leq 7.25) = 1 - 1 = 0$

5-8. 95% level of confidence,  $E = 1$ , and  $z_{0.025} = 1.96$

$$n \cong \left( \frac{z_{0.025}}{E} \right)^2 (\sigma_1^2 + \sigma_2^2) = \left( \frac{1.96}{1} \right)^2 (1.5 + 1.2) = 10.37, n = 11, \text{ use } n_1 = n_2 = 11$$

5-10.	<u>Catalyst 1</u>	<u>Catalyst 2</u>
	$\bar{x}_1 = 65.22$	$\bar{x}_2 = 68.42$
	$\sigma_1 = 3$	$\sigma_2 = 3$
	$n_1 = 10$	$n_2 = 10$

a) 95% confidence interval on  $\mu_1 - \mu_2$ , the difference in mean active concentration

$$(\bar{x}_1 - \bar{x}_2) - z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}} \leq \mu_1 - \mu_2 \leq (\bar{x}_1 - \bar{x}_2) + z_{\alpha/2} \sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}$$

$$(65.22 - 68.42) - 1.96 \sqrt{\frac{(3)^2}{10} + \frac{(3)^2}{10}} \leq \mu_1 - \mu_2 \leq (65.22 - 68.42) + 1.96 \sqrt{\frac{(3)^2}{10} + \frac{(3)^2}{10}}$$

$$-5.83 \leq \mu_1 - \mu_2 \leq -0.57$$

We are 95% confident that the mean active concentration of catalyst 2 exceeds that of catalyst 1 by between 0.57 and 5.83 g/l.

b) Yes, since the 95% confidence interval did not contain the value 0, we would conclude the mean active concentration depends on the choice of catalyst.

- 5-12.
- 1) The parameter of interest is the difference in mean active concentration,  $\mu_1 - \mu_2$
  - 2)  $H_0 : \mu_1 - \mu_2 = 0$  or  $\mu_1 = \mu_2$
  - 3)  $H_1 : \mu_1 - \mu_2 \neq 0$  or  $\mu_1 \neq \mu_2$
  - 4)  $\alpha = 0.05$
  - 5) The test statistic is

$$z_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{\sqrt{\frac{\sigma_1^2}{n_1} + \frac{\sigma_2^2}{n_2}}}$$

6) Reject  $H_0$  if  $z_0 < -z_{\alpha/2} = -1.96$  or  $z_0 > z_{\alpha/2} = 1.96$

7)  $\bar{x}_1 = 750.2$   $\bar{x}_2 = 756.88$   $\delta = 0$

$$\sigma_1 = 20 \quad \sigma_2 = 20$$

$$n_1 = 15 \quad n_2 = 8$$

$$z_0 = \frac{(750.2 - 756.88) - 0}{\sqrt{\frac{(20)^2}{15} + \frac{(20)^2}{8}}} = -2.385$$

8) Since  $-2.385 < -1.96$  reject the null hypothesis and conclude the mean active concentrations do differ significantly at  $\alpha = 0.05$ .

$$P\text{-value} = 2(1 - \Phi(2.385)) = 2(1 - 0.99146) = 0.0171$$

The conclusions reached by the confidence interval of problem 5-10 and the test of hypothesis conducted here are the same. A two-sided confidence interval can be thought of as representing the "acceptance region" of a hypothesis test, given that the level of significance is the same for both procedures. Thus if the value  $\delta$  falls outside the confidence interval, it is the same result as rejecting the null hypothesis.

5-14. Assume the populations follow normal distributions and  $\sigma_1^2 = \sigma_2^2$ . The assumption of equal variances may be permitted in this case since it is known that the t-test and confidence intervals involving the t-distribution are robust to this assumption of equal variances when sample sizes are equal.

Case 1: AFCC

Case 2: ATC

$\mu_1$  = mean foam expansion for AFCC

$$\bar{x}_1 = 4.7$$

$$s_1 = 0.6$$

$$n_1 = 5$$

$\mu_2$  = mean foam expansion for ATC

$$\bar{x}_2 = 6.9$$

$$s_2 = 0.8$$

$$n_2 = 5$$

95% confidence interval:  $t_{0.025,8} = 2.306$

$$s_p = \sqrt{\frac{5(0.60) + 5(0.80)}{8}} = 0.7071$$

$$(\bar{x}_1 - \bar{x}_2) - t_{\alpha/2, n_1 + n_2 - 2}(s_p) \sqrt{\frac{1}{n_1} + \frac{1}{n_2}} \leq \mu_1 - \mu_2 \leq (\bar{x}_1 - \bar{x}_2) + t_{\alpha/2, n_1 + n_2 - 2}(s_p) \sqrt{\frac{1}{n_1} + \frac{1}{n_2}}$$

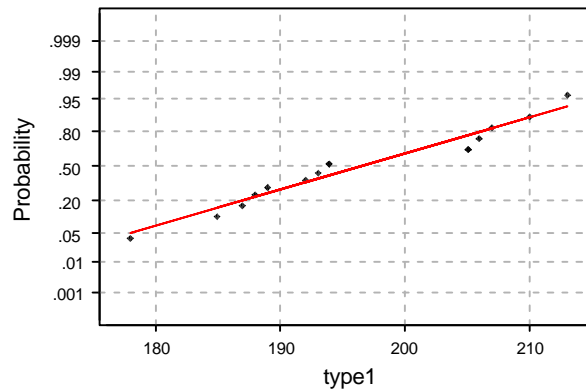
$$(4.7 - 6.9) - 2.306 \sqrt{\frac{1}{5} + \frac{1}{5}} \leq \mu_1 - \mu_2 \leq (4.7 - 6.9) + 2.306 \sqrt{\frac{1}{5} + \frac{1}{5}}$$

$$-3.23 \leq \mu_1 - \mu_2 \leq -1.17$$

Yes, with 95% confidence, we believe the mean foam expansion for ATC exceeds that of AFCC by between 1.17 and 2.32.

- 5-16. a) According to the normal probability plots, the assumption of normality appears to be met since the data fall approximately along a straight line. The equality of variances does not appear to be severely violated either since the slopes are approximately the same for both samples.

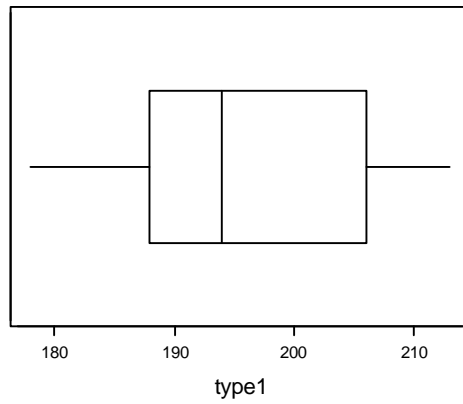
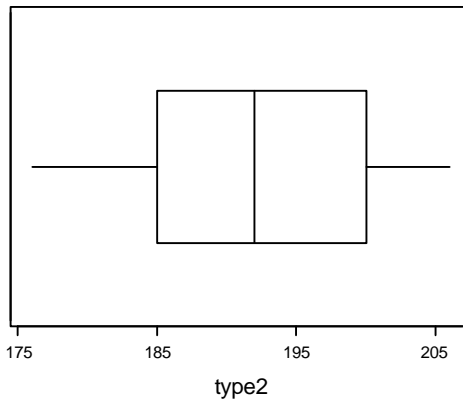
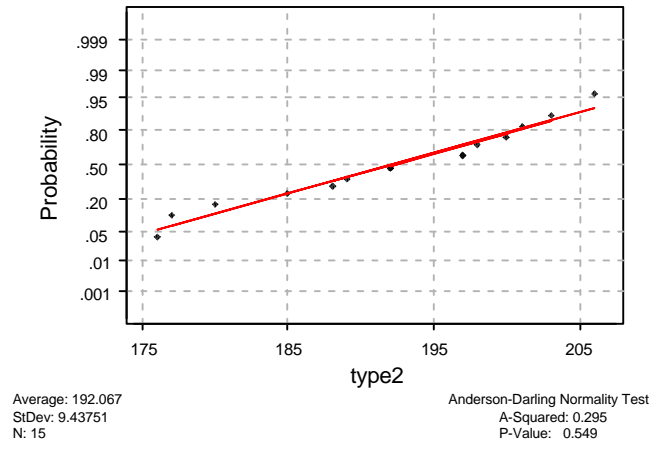
#### Normal Probability Plot



Average: 196.4  
StDev: 10.4799  
N: 15

Anderson-Darling Normality Test  
A-Squared: 0.463  
P-Value: 0.220

Normal Probability Plot



b) 1) The parameter of interest is the difference in deflection temperature under load,  $\mu_1 - \mu_2$

- 2)  $H_0 : \mu_1 - \mu_2 = 0$  or  $\mu_1 = \mu_2$
- 3)  $H_1 : \mu_1 - \mu_2 < 0$  or  $\mu_1 < \mu_2$
- 4)  $\alpha = 0.05$
- 5) The test statistic is

$$t_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{s_p \sqrt{\frac{1}{n_1} + \frac{1}{n_2}}}$$

- 6) Reject the null hypothesis if  $t_0 < -t_{\alpha, n_1 + n_2 - 2}$  where  $-t_{0.05, 28} = -1.701$

- 7) Type 1                      Type 2

$$\begin{aligned} \bar{x}_1 = 196.4 \quad \bar{x}_2 = 192.067 \quad \Delta_0 = 0 \quad s_p &= \sqrt{\frac{(n_1 - 1)s_1^2 + (n_2 - 1)s_2^2}{n_1 + n_2 - 2}} \\ s_1 = 10.48 \quad s_2 = 9.44 &= \sqrt{\frac{14(10.48)^2 + 14(9.44)^2}{28}} = 9.97 \\ n_1 = 15 \quad n_2 = 15 & \\ t_0 &= \frac{(196.4 - 192.067) - 0}{9.97 \sqrt{\frac{1}{15} + \frac{1}{15}}} = 1.19 \end{aligned}$$

- 8) Since  $1.19 > -1.701$  do not reject the null hypothesis and conclude the mean deflection temperature under load for type 2 does not significantly exceed the mean deflection temperature under load for type 1 at the 0.05 level of significance.

c) P-value =  $2P(t > 1.19)$      $0.75 < \text{p-value} < 0.90$

- d)  $\Delta = 5$     Use  $s_p$  as an estimate of  $\sigma$ :

$$d = \frac{\mu_2 - \mu_1}{2s_p} = \frac{5}{2(9.97)} = 0.251$$

Using Chart V g) with  $\beta = 0.10$ ,  $d = 0.251$  we get  $n \cong 100$ . So,  $n_1 = n_2 = 100$ ; Therefore, the sample sizes of 15 are inadequate.

- 5-18. a) 1) The parameter of interest is the difference in mean impact strength,  $\mu_1 - \mu_2$

- 2)  $H_0 : \mu_1 - \mu_2 = 0$  or  $\mu_1 = \mu_2$
- 3)  $H_1 : \mu_1 - \mu_2 < 0$  or  $\mu_1 < \mu_2$
- 4)  $\alpha = 0.05$
- 5) The test statistic is

$$t_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{\sqrt{\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}}}$$

- 6) Reject the null hypothesis if  $t_0 < -t_{\alpha, v}$  where  $t_{0.05, 25} = -1.708$  since

$$v = \frac{\left(\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}\right)^2}{\frac{\left(\frac{s_1^2}{n_1}\right)^2}{n_1 + 1} + \frac{\left(\frac{s_2^2}{n_2}\right)^2}{n_2 + 1}} - 2 = 27.43 - 2 = 25.43$$

$v \cong 25$   
(truncated)

7)  $\bar{x}_1 = 290$      $\bar{x}_2 = 321$

$$s_1 = 12 \quad s_2 = 22$$

$$n_1 = 10 \quad n_2 = 16$$

$$t_0 = \frac{(290 - 321) - 0}{\sqrt{\frac{(12)^2}{10} + \frac{(22)^2}{16}}} = -4.64$$

8) Since  $-4.64 < -1.708$  reject the null hypothesis and conclude that supplier 2 provides gears with higher mean impact strength at the 0.05 level of significance.

b) P-value =  $P(t < -4.64)$ : P-value  $< 0.0005$

c) 1) The parameter of interest is the difference in mean impact strength,  $\mu_2 - \mu_1$

2)  $H_0 : \mu_2 - \mu_1 = 25$

3)  $H_1 : \mu_2 - \mu_1 > 25$  or  $\mu_2 > \mu_1 + 25$

4)  $\alpha = 0.05$

5) The test statistic is

$$t_0 = \frac{(\bar{x}_2 - \bar{x}_1) - \delta}{\sqrt{\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}}}$$

6) Reject the null hypothesis if  $t_0 > t_{\alpha, v} = 1.708$  where

$$v = \frac{\left(\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}\right)^2}{\frac{\left(\frac{s_1^2}{n_1}\right)^2}{n_1 + 1} + \frac{\left(\frac{s_2^2}{n_2}\right)^2}{n_2 + 1}} - 2 = 27.43 - 2 = 25.43$$

$$v \cong 25$$

7)  $\bar{x}_1 = 290 \quad \bar{x}_2 = 321 \quad \Delta_0 = 25$

$$s_1 = 12 \quad s_2 = 22$$

$$n_1 = 10 \quad n_2 = 16$$

$$t_0 = \frac{(321 - 290) - 25}{\sqrt{\frac{(12)^2}{10} + \frac{(22)^2}{16}}} = 0.898$$

8) Since  $0.898 < 1.708$ , do not reject the null hypothesis and conclude that the mean impact strength from supplier 2 is not at least 25 ft-lb higher than supplier 1 using  $\alpha = 0.05$ .

5-20. 1) The parameter of interest is the difference in mean melting point,  $\mu_1 - \mu_2$

2)  $H_0 : \mu_1 - \mu_2 = 0$  or  $\mu_1 = \mu_2$

3)  $H_1 : \mu_1 - \mu_2 \neq 0$  or  $\mu_1 \neq \mu_2$

4)  $\alpha = 0.02$

5) The test statistic is

$$t_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{s_p \sqrt{\frac{1}{n_1} + \frac{1}{n_2}}}$$

6) Reject the null hypothesis if  $t_0 < -t_{\alpha/2, n_1 + n_2 - 2}$  where  $-t_{0.01, 40} = -2.423$  or  $t_0 > t_{\alpha/2, n_1 + n_2 - 2}$  where

$$t_{0.01, 40} = 2.423$$

7)  $\bar{x}_1 = 421 \quad \bar{x}_2 = 426 \quad \Delta_0 = 0 \quad s_p = \sqrt{\frac{(n_1 - 1)s_1^2 + (n_2 - 1)s_2^2}{n_1 + n_2 - 2}}$

$$s_1 = 4 \quad s_2 = 3 \quad = \sqrt{\frac{20(4)^2 + 20(3)^2}{40}} = 2.915$$

$$n_1 = 21 \quad n_2 = 21$$

$$t_0 = \frac{(421 - 426) - 0}{2.915 \sqrt{\frac{1}{20} + \frac{1}{20}}} = -5.424$$

8) Since  $-5.424 < -2.423$  reject the null hypothesis and conclude that the data do not support the claim that both alloys have the same melting point at  $\alpha = 0.02$

$$P\text{-value} = 2P(t < -5.424) \quad P\text{-value} < 0.0010$$

5-22. a) 1) The parameter of interest is the difference in mean wear amount,  $\mu_1 - \mu_2$ .

2)  $H_0: \mu_1 - \mu_2 = 0$  or  $\mu_1 = \mu_2$

3)  $H_1: \mu_1 - \mu_2 \neq 0$  or  $\mu_1 \neq \mu_2$

4)  $\alpha = 0.05$

5) The test statistic is

$$t_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{\sqrt{\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}}}$$

6) Reject the null hypothesis if  $t_0 < -t_{0.025,27}$  where  $-t_{0.025,27} = -2.052$  or  $t_0 > t_{0.025,27}$  where

$$t_{0.025,27} =$$

2.052 since

$$v = \frac{\left(\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}\right)^2}{\frac{\left(\frac{s_1^2}{n_1}\right)^2}{n_1 + 1} + \frac{\left(\frac{s_2^2}{n_2}\right)^2}{n_2 + 1}} - 2 = 29.24 - 2 = 27.43$$

$$v \cong 27$$

(truncated)

7)  $\bar{x}_1 = 20 \quad \bar{x}_2 = 15$

$\Delta_0 = 0$

$s_1 = 2 \quad s_2 = 8$

$n_1 = 25 \quad n_2 = 25$

$$t_0 = \frac{(20 - 15) - 0}{\sqrt{\frac{(2)^2}{25} + \frac{(8)^2}{25}}} = 3.03$$

8) Since  $3.03 > 2.052$  reject the null hypothesis and conclude that the data support the claim that the two companies produce material with significantly different wear at the 0.05 level of significance.

b)  $P\text{-value} = 2P(t > 3.03), \quad 2(0.0025) < P\text{-value} < 2(0.005)$

$$0.005 < P\text{-value} < 0.010$$

c) 1) The parameter of interest is the difference in mean wear amount,  $\mu_1 - \mu_2$

2)  $H_0: \mu_1 - \mu_2 = 0$

3)  $H_1: \mu_1 - \mu_2 > 0$

4)  $\alpha = 0.05$

5) The test statistic is

$$t_0 = \frac{(\bar{x}_1 - \bar{x}_2) - \Delta_0}{\sqrt{\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}}}$$

6) Reject the null hypothesis if  $t_0 > t_{0.05,27}$  where  $t_{0.05,27} = 1.703$  since

$$v = \frac{\left(\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}\right)^2}{\frac{\left(\frac{s_1^2}{n_1}\right)^2}{n_1+1} + \frac{\left(\frac{s_2^2}{n_2}\right)^2}{n_2+1}} - 2 = 29.24 - 2 = 27.43$$

$$v \cong 27$$

7)  $\bar{x}_1 = 20$     $\bar{x}_2 = 15$

$s_1 = 2$     $s_2 = 8$     $\Delta_0 = 0$   
 $n_1 = 25$     $n_2 = 25$

$$t_0 = \frac{(20-15)-0}{\sqrt{\frac{(2)^2}{25} + \frac{(8)^2}{25}}} = 3.03$$

8) Since  $3.03 > 1.703$  reject the null hypothesis and conclude that the data support the claim that the material from company 1 has a higher mean wear than the material from company 2 using a 0.05 level of significance.

5-24. If  $\alpha = 0.01$ , construct a 99% lower one-sided confidence interval on the difference to answer this question.  
 $t_{0.01,19} = 2.539$

$$(\bar{x}_1 - \bar{x}_2) - t_{\alpha,v} \sqrt{\frac{s_1^2}{n_1} + \frac{s_2^2}{n_2}} \leq \mu_1 - \mu_2$$

$$(1035 - 99.7) - 2.539 \sqrt{\frac{(10.2)^2}{12} + \frac{(20.1)^2}{13}} \leq \mu_1 - \mu_2$$

$$-12.21 \leq \mu_1 - \mu_2 .$$

Since the interval contains 0, we are 99% confident there is no difference in the mean coating thickness between the two temperatures; that is, raising the process temperature does not significantly reduce the mean coating thickness.

5-26.  $\bar{d} = 0.2736$     $s_d = 0.1356$ ,  $n = 9$   
 95% confidence interval:

$$\bar{d} - t_{\alpha/2, n-1} \left( \frac{s_d}{\sqrt{n}} \right) \leq \mu_d \leq \bar{d} + t_{\alpha/2, n-1} \left( \frac{s_d}{\sqrt{n}} \right)$$

$$0.2736 - 2.306 \left( \frac{0.1356}{\sqrt{9}} \right) \leq \mu_d \leq 0.2736 + 2.306 \left( \frac{0.1356}{\sqrt{9}} \right)$$

$$0.1694 \leq \mu_d \leq 0.3778$$

With 95% confidence, we believe the mean shear strength of Karlsruhe method exceeds the mean shear strength of the Lehigh method by between 0.1714 and 0.3758. Since 0 is not included in this interval, the interval is consistent with rejecting the null hypothesis that the means are the same.

The 95% confidence interval is directly related to a test of hypothesis with 0.05 level of significance, and the conclusions reached are identical.

5-28. 1) The parameter of interest is the difference between the mean parking times,  $\mu_d$ .

- 2)  $H_0 : \mu_d = 0$
- 3)  $H_1 : \mu_d \neq 0$
- 4)  $\alpha = 0.10$
- 5) The test statistic is

$$t_0 = \frac{\bar{d}}{s_d / \sqrt{n}}$$

- 6) Reject the null hypothesis if  $t_0 < -t_{0.05,13}$  where  $-t_{0.05,13} = -1.771$  or  $t_0 > t_{0.05,13}$  where  $t_{0.05,13} = 1.771$

- 7)  $\bar{d} = 1.21$   
 $s_d = 12.68$   
 $n = 14$

$$t_0 = \frac{1.21}{12.68 / \sqrt{14}} = 0.357$$

- 8) Since  $-1.771 < 0.357 < 1.771$  do not reject the null and conclude the data do not support the claim that two cars have different mean parking times at the 0.10 level of significance. The result is consistent with the confidence interval constructed since 0 is included in the 90% confidence interval.

- 5-30.  $\bar{d} = 868.375$   $s_d = 1290$ ,  $n = 8$  where  $d_i = \text{brand 1} - \text{brand 2}$   
 99% confidence interval:

$$\bar{d} - t_{\alpha/2, n-1} \left( \frac{s_d}{\sqrt{n}} \right) \leq \mu_d \leq \bar{d} + t_{\alpha/2, n-1} \left( \frac{s_d}{\sqrt{n}} \right)$$

$$868.375 - 3.499 \left( \frac{1290}{\sqrt{8}} \right) \leq \mu_d \leq 868.375 + 3.499 \left( \frac{1290}{\sqrt{8}} \right)$$

$$-727.46 \leq \mu_d \leq 2464.21$$

Since zero is contained within this interval, we are 99% confident there is no significant difference between the two brands of tire.

- 5-32. 1) The parameter of interest is the difference in blood cholesterol level,  $\mu_d$  where  $d_i = \text{Before} - \text{After}$ .
- 2)  $H_0 : \mu_d = 0$
  - 3)  $H_1 : \mu_d > 0$
  - 4)  $\alpha = 0.05$
  - 5) The test statistic is

$$t_0 = \frac{\bar{d}}{s_d / \sqrt{n}}$$

- 6) Reject the null hypothesis if  $t_0 > t_{0.05,14}$  where  $t_{0.05,14} = 1.761$

- 7)  $\bar{d} = 26.867$   
 $s_d = 19.04$   
 $n = 15$

$$t_0 = \frac{26.867}{19.04 / \sqrt{15}} = 5.465$$

- 8) Since  $5.465 > 1.761$  reject the null and conclude the data support the claim that low the mean difference in cholesterol levels is significantly less after fat diet and aerobic exercise program at the 0.05 level of significance.

- 5-34. 1) The parameter of interest is the difference in mean weight,  $\mu_d$  where  $d_i = \text{Weight Before} - \text{Weight After}$ .
- 2)  $H_0 : \mu_d = 0$
  - 3)  $H_1 : \mu_d > 0$
  - 4)  $\alpha = 0.05$
  - 5) The test statistic is



$$s_1 = 4.7 \quad s_2 = 5.8$$

$$f_0 = \frac{(4.7)^2}{(5.8)^2} = 0.657$$

8) Since  $0.265 < 0.657 < 3.12$  do not reject the null hypothesis and conclude there is insufficient evidence to indicate the two population variances differ significantly at the 0.05 level of significance.

5-42. a) 90% confidence interval for the ratio of variances:

$$\left( \frac{s_1^2}{s_2^2} \right) f_{1-\alpha/2, n_1-1, n_2-1} \leq \frac{\sigma_1^2}{\sigma_2^2} \leq \left( \frac{s_1^2}{s_2^2} \right) f_{\alpha/2, n_1-1, n_2-1}$$

$$\left( \frac{(0.35)^2}{(0.40)^2} \right) 0.412 \leq \frac{\sigma_1^2}{\sigma_2^2} \leq \left( \frac{(0.35)^2}{(0.40)^2} \right) 2.33$$

$$0.3605 \leq \frac{\sigma_1^2}{\sigma_2^2} \leq 2.039$$

Since the interval contains 1, we are 90% confident the variances for the rod diameters are not significantly different.

b) 95% confidence interval:

$$\left( \frac{s_1^2}{s_2^2} \right) f_{1-\alpha/2, n_1-1, n_2-1} \leq \frac{\sigma_1^2}{\sigma_2^2} \leq \left( \frac{s_1^2}{s_2^2} \right) f_{\alpha/2, n_1-1, n_2-1}$$

$$\left( \frac{(0.35)^2}{(0.40)^2} \right) 0.345 \leq \frac{\sigma_1^2}{\sigma_2^2} \leq \left( \frac{(0.35)^2}{(0.40)^2} \right) 2.75$$

$$0.302 \leq \frac{\sigma_1^2}{\sigma_2^2} \leq 2.406$$

We are 95% confident the variances for the rod diameters are not significantly different.

The 95% confidence interval is wider than the 90% confidence interval.

c) 90% lower-sided confidence interval:

$$\left( \frac{s_1^2}{s_2^2} \right) f_{1-\alpha, n_1-1, n_2-1} \leq \frac{\sigma_1^2}{\sigma_2^2}$$

$$\left( \frac{(0.35)^2}{(0.40)^2} \right) 0.503 \leq \frac{\sigma_1^2}{\sigma_2^2}$$

$$0.440 \leq \frac{\sigma_1^2}{\sigma_2^2}$$

With 90% confidence, we believe the variances for the rod diameters are not significantly different from each other.

5-44. 1) The parameters of interest are the thickness variances,  $\sigma_1^2, \sigma_2^2$

2)  $H_0 : \sigma_1^2 = \sigma_2^2$

3)  $H_1 : \sigma_1^2 \neq \sigma_2^2$

4)  $\alpha = 0.02$

5) The test statistic is

$$f_0 = \frac{s_1^2}{s_2^2}$$

6) Reject the null hypothesis if  $f_0 < f_{0.99, 7, 7}$  where  $f_{0.99, 7, 7} = 0.143$  or  $f_0 > f_{0.01, 7, 7}$  where  $f_{0.01, 7, 7} = 6.99$

7)  $n_1 = 8 \quad n_2 = 8$

$$s_1 = 0.11 \quad s_2 = 0.09$$

$$f_0 = \frac{(0.11)^2}{(0.09)^2} = 1.49$$

8) Since  $0.143 < 1.232 < 6.99$  do not reject the null hypothesis and conclude the thickness variances do not significantly differ at the 0.02 level of significance.

5-46. 1) The parameters of interest are the melting variances,  $\sigma_1^2, \sigma_2^2$

2)  $H_0 : \sigma_1^2 = \sigma_2^2$

3)  $H_1 : \sigma_1^2 \neq \sigma_2^2$

4)  $\alpha = 0.05$

5) The test statistic is

$$f_0 = \frac{s_1^2}{s_2^2}$$

6) Reject the null hypothesis if  $f_0 < f_{0.975,20,20}$  where  $f_{0.975,20,20} = 0.4065$  or  $f_0 > f_{0.025,20,20}$  where  $f_{0.025,20,20} = 2.46$

7)  $n_1 = 21 \quad n_2 = 21$

$s_1 = 4 \quad s_2 = 3$

$$f_0 = \frac{(4)^2}{(3)^2} = 1.78$$

8) Since  $0.4065 < 1.78 < 2.46$  do not reject the null hypothesis and conclude the population variances do not significantly differ at the 0.05 level of significance.

5-48. 1) The parameters of interest are the time to assemble standard deviations,  $\sigma_1, \sigma_2$

2)  $H_0 : \sigma_1^2 = \sigma_2^2$

3)  $H_1 : \sigma_1^2 \neq \sigma_2^2$

4)  $\alpha = 0.02$

5) The test statistic is

$$f_0 = \frac{s_1^2}{s_2^2}$$

6) Reject the null hypothesis if  $f_0 < f_{1-\alpha/2, n_1-1, n_2-1} = 0.365$  or  $f_0 > f_{\alpha/2, n_1-1, n_2-1} = 2.86$

7)  $n_1 = 25 \quad n_2 = 21$

$s_1 = 0.98 \quad s_2 = 1.02$

$$f_0 = \frac{(1.02)^2}{(0.98)^2} = 0.923$$

8) Since  $0.365 < 0.923 < 2.86$  do not reject the null hypothesis and conclude there is no evidence to support the claim that men and women differ significantly in repeatability for this assembly task at the 0.02 level of significance.

5-50. 1) the parameters of interest are the proportion of defective parts,  $p_1$  and  $p_2$

2)  $H_0 : p_1 = p_2$

3)  $H_1 : p_1 \neq p_2$

4)  $\alpha = 0.05$

5) Test statistic is

$$z_0 = \frac{\hat{p}_1 - \hat{p}_2}{\sqrt{\hat{p}(1-\hat{p})\left(\frac{1}{n_1} + \frac{1}{n_2}\right)}} \quad \text{where}$$

$$\hat{p} = \frac{x_1 + x_2}{n_1 + n_2}$$

6) Reject the null hypothesis if  $z_0 < -z_{0.025}$  where  $-z_{0.025} = -1.96$  or  $z_0 > z_{0.025}$  where  $z_{0.025} = 1.96$

7)  $n_1 = 300$        $n_2 = 300$   
 $x_1 = 15$        $x_2 = 8$

$$\hat{p}_1 = 0.05 \quad \hat{p}_2 = 0.0267 \quad \hat{p} = \frac{15+8}{300+300} = 0.0383$$

$$z_0 = \frac{0.05 - 0.0267}{\sqrt{0.0383(1-0.0383)\left(\frac{1}{300} + \frac{1}{300}\right)}} = 1.49$$

8) Since  $-1.96 < 1.49 < 1.96$  do not reject the null hypothesis and conclude that yes the evidence indicates that there is not a significant difference in the fraction of defective parts produced by the two machines at the 0.05 level of significance.

$$P\text{-value} = 2(1 - P(z < 1.49)) = 0.13622$$

5-52. a)  $\beta = \Phi\left(\frac{z_{\alpha/2} \sqrt{\bar{p}\bar{q}\left(\frac{1}{n_1} + \frac{1}{n_2}\right)} - (p_1 - p_2)}{\hat{\sigma}_{\hat{p}_1 - \hat{p}_2}}\right) - \Phi\left(\frac{-z_{\alpha/2} \sqrt{\bar{p}\bar{q}\left(\frac{1}{n_1} + \frac{1}{n_2}\right)} - (p_1 - p_2)}{\hat{\sigma}_{\hat{p}_1 - \hat{p}_2}}\right)$

$$\bar{p} = \frac{300(0.05) + 300(0.02)}{300 + 300} = 0.035 \quad \bar{q} = 0.965$$

$$\hat{\sigma}_{\hat{p}_1 - \hat{p}_2} = \sqrt{\frac{0.05(1-0.05)}{300} + \frac{0.02(1-0.02)}{300}} = 0.015$$

$$\beta = \Phi\left(\frac{1.96 \sqrt{0.035(0.965)\left(\frac{1}{300} + \frac{1}{300}\right)} - (0.05 - 0.02)}{0.015}\right) - \Phi\left(\frac{-1.96 \sqrt{0.035(0.965)\left(\frac{1}{300} + \frac{1}{300}\right)} - (0.05 - 0.02)}{0.015}\right)$$

$$= \Phi(-0.04) - \Phi(-3.96) = 0.48405 - 0.00004 = 0.48401$$

$$\text{Power} = 1 - 0.48401 = 0.51599$$

$$b) n = \frac{\left(z_{\alpha/2} \sqrt{\frac{(p_1 + p_2)(q_1 + q_2)}{2}} + z_{\beta} \sqrt{p_1 q_1 + p_2 q_2}\right)^2}{(p_1 - p_2)^2}$$

$$= \frac{\left(1.96 \sqrt{\frac{(0.05 + 0.02)(0.95 + 0.98)}{2}} + 1.29 \sqrt{0.05(0.95) + 0.02(0.98)}\right)^2}{(0.05 - 0.02)^2} = 790.67$$

$$n = 791$$

5-54. 95% confidence interval on the difference:

$$(\hat{p}_1 - \hat{p}_2) - z_{\alpha/2} \sqrt{\frac{\hat{p}_1(1-\hat{p}_1)}{n_1} + \frac{\hat{p}_2(1-\hat{p}_2)}{n_2}} \leq p_1 - p_2 \leq (\hat{p}_1 - \hat{p}_2) + z_{\alpha/2} \sqrt{\frac{\hat{p}_1(1-\hat{p}_1)}{n_1} + \frac{\hat{p}_2(1-\hat{p}_2)}{n_2}}$$

$$(0.05 - 0.0267) - 1.96 \sqrt{\frac{0.05(1-0.05)}{300} + \frac{0.0267(1-0.0267)}{300}} \leq p_1 - p_2 \leq (0.05 - 0.0267) + 1.96 \sqrt{\frac{0.05(1-0.05)}{300} + \frac{0.0267(1-0.0267)}{300}}$$

$$-0.0074 \leq p_1 - p_2 \leq 0.054$$

Since this interval contains the value zero, we are 95% confident there is no significant difference in the fraction of defective parts produced by the two machines and that the difference in proportions is between -0.0074 and 0.054.

5-56. a)

One-Way Analysis of Variance

-----  
Data: Observation

Level codes: SCCM

Labels:

Means plot: LSD

Confidence level: 90

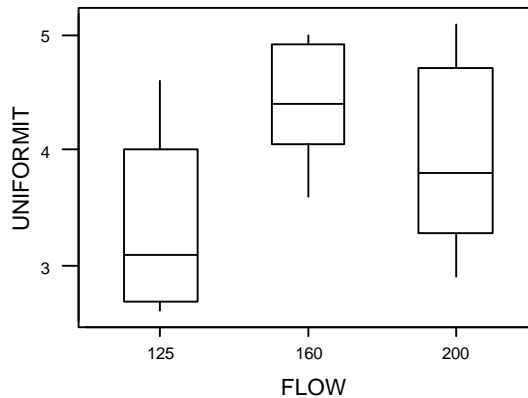
Range test: LSD

Analysis of variance

Source of variation level	Sum of Squares	d.f.	Mean square	F-ratio	Sig.
Between groups	3.6477778	2	1.8238889	3.586	.0534
Within groups	7.6300000	15	.5086667		
Total (corrected)	11.277778	17			

0 missing value(s) have been excluded.

Reject  $H_0$  at  $\alpha = 0.01$ .  $C_2F_6$  flow rate does appear to affect etch uniformity.



b) Examining the box plots, the 125 and 160 mean levels seem to be the most different.

5-58. a)

One-Way Analysis of Variance

-----  
Data: Density

Level codes: Temp

Labels:

Means plot: LSD

Confidence level: 95

Range test: LSD

Analysis of variance

Source of variation level	Sum of Squares	d.f.	Mean square	F-ratio	Sig.
Between groups	.1391104	3	.0463701	2.616	.0827
Within groups	.3190714	18	.0177262		
Total (corrected)	.4581818	21			

0 missing value(s) have been excluded.

Do not reject  $H_0$ . There is insignificant evidence to indicate the four firing temperatures affect the density of the brick.

b) P-value = 0.0827

5-60.

One-Way Analysis of Variance

Data: Conductivity

Level codes: Coating

Labels:

Means plot: LSD

Confidence level: 95

Range test: LSD

Analysis of variance

Source of variation level	Sum of Squares	d.f.	Mean square	F-ratio	Sig.
Between groups	1060.5000	4	265.12500	16.349	.0000
Within groups	243.2500	15	16.21667		
Total (corrected)	1303.7500	19			

0 missing value(s) have been excluded.

Reject  $H_0$ . There appears to be a significant difference among the five coating types in their effect on conductivity.

## Chapter 6 (Section 6.1-6.4)

6-2. a)  $y_0 = \beta_0 + \beta_1 x_1$

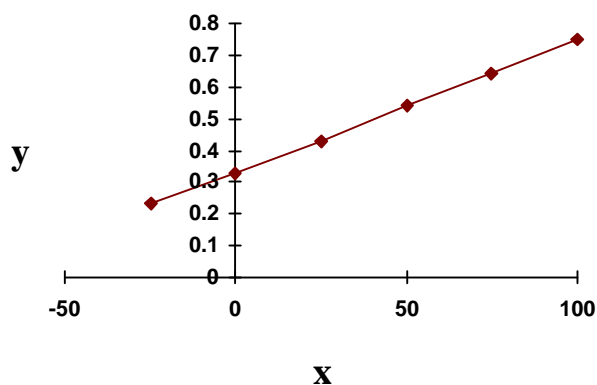
$$S_{xx} = 143215.8 - \frac{1478^2}{20} = 33991.6$$

$$S_{xy} = 1083.67 - \frac{(1478)(12.75)}{20} = 141.445$$

$$\hat{\beta}_1 = \frac{S_{xy}}{S_{xx}} = \frac{141.445}{33991.6} = 0.0041612$$

$$\hat{\beta}_0 = \frac{12.75}{20} - (0.0041612)\left(\frac{1478}{20}\right) = 0.3299892$$

$$\hat{y} = 0.3299892 + 0.0041612x$$



b)  $\hat{y} = 0.3299892 + 0.0041612(85) = 0.683689$

c)  $\hat{y} = 0.3299892 + 0.0041612(90) = 0.7044949$

d)  $\hat{\beta}_1 = 0.00416$

6-4. a)  
Regression Analysis - Linear model:  $Y = a + bX$

Dependent variable: Games		Independent variable: Yards			
Parameter	Estimate	Standard Error	T Value	Prob. Level	
Intercept	21.7883	2.69623	8.081	.00000	
Slope	-7.0251E-3	1.25965E-3	-5.57703	.00001	
Analysis of Variance					
Source	Sum of Squares	Df	Mean Square	F-Ratio	Prob. Level
Model	178.09231	1	178.09231	31.1032	.00001
Residual	148.87197	26	5.72585		
Total (Corr.)		326.96429	27		
Correlation Coefficient = -0.738027			R-squared = 54.47 percent		
Std. Error of Est. = 2.39287					



$$d) \hat{y} = -6.3355 + 9.20836(47) = 426.458$$

$$\hat{y} = 426.458$$

$$e = y - \hat{y} = 424.84 - 426.458 = -1.618$$

6-8.

Model fitting results for: y

Independent variable sig.level	coefficient	std. error	t-value
CONSTANT 0.0183	350.994271	74.753074	4.6954
x1 0.3562	-1.271994	1.16914	-1.0880
x2 0.1841	-0.153904	0.08953	-1.7190

R-SQ. (ADJ.) = 0.7696 SE= 25.497858 MAE= 16.319125 DurbWat= 2.565  
 Previously: 0.0000 0.000000 0.000000  
 6 observations fitted, forecast(s) computed for 0 missing val. of dep. var.

If the calculations were to be done by hand use Equation (6-21).

a)  $\hat{y} = 350.9943 - 1.272x_1 - 0.1539x_2$

b)  $\hat{y} = 350.9943 - 1.272(25) - 0.1539(1000) = 165.29$

c)

Model fitting results for: y

Independent variable sig.level	coefficient	std. error	t-value
CONSTANT 0.5899	125.865548	197.957166	0.6358
x1 0.4104	7.758641	7.514795	1.0324
x2 0.7107	0.094304	0.220657	0.4274
x1*x2 0.3485	0.009186	0.007564	-1.2145

R-SQ. (ADJ.) = 0.8011 SE= 23.691404 MAE= 12.527757 DurbWat= 3.003  
 Previously: 0.7696 25.497858 16.319125  
 6 observations fitted, forecast(s) computed for 0 missing val. of dep. var.

If the calculations were to be done by hand, add a cross-product column to the **X** matrix and use Equation (6-21).

$$\hat{y}' = 125.8655 - 7.7586x_1 - 0.0943x_2 - 0.0092x_1x_2$$

d)  $\hat{y}' = 125.8655 - 7.7586(25) - 0.0943(1000) - 0.0092(25)(1000)$   
 $\hat{y}' = 184.13$  The predicted value is larger

6-10.

Model fitting results for: y

Independent variable sig.level	coefficient	std. error	t-value
CONSTANT 0.3555	47.173999	49.581476	0.9514
x1 0.0179	-9.735202	3.691625	-2.6371
x2 0.0739	0.428287	0.223933	1.9126
x3 0.0000	18.237455	1.311802	13.9026

R-SQ. (ADJ.) = 0.9925 SE= 3.479627 MAE= 2.511105 DurbWat= 1.778  
Previously: 0.0000 0.000000 0.000000  
0.000  
20 observations fitted, forecast(s) computed for 0 missing val. of dep. var.

If the calculations were to be done by hand, add a cross-product column to the  $\mathbf{X}$  matrix and use Equation (6-21).

- a)  $\hat{y} = 47.174 - 9.7352x_1 + 0.4283x_2 + 18.2375x_3$   
b)  $\hat{y} = 47.174 - 9.7352(14.5) + 0.4283(220) + 18.2375(5) = 91.43$

- 6-12. a) 1) The parameter of interest is the regressor variable coefficient,  $\beta_1$   
2)  $H_0: \beta_1 = 0$   
3)  $H_1: \beta_1 \neq 0$   
4)  $\alpha = 0.05$   
5) The test statistic is

$$f_0 = \frac{MS_R}{MS_E} = \frac{SS_R / 1}{SS_E / (n - 2)}$$

- 6) Reject  $H_0$  if  $f_0 > f_{\alpha, 1, 12}$  where  $f_{0.05, 1, 12} = 4.75$   
7) Using results from Exercise 6-1

$$\begin{aligned} SS_R &= \hat{\beta}_1 S_{xy} = -2.3298017(-59.057143) \\ &= 137.59 \\ SS_E &= S_{yy} - SS_R \\ &= 159.71429 - 137.59143 \\ &= 22.123 \end{aligned}$$

$$f_0 = \frac{137.59}{22.123 / 12} = 74.63$$

8) Since  $74.63 > 4.75$  reject  $H_0$  and conclude that compressive strength is a significant in predicting intrinsic permeability of concrete at  $\alpha = 0.05$ . We can therefore conclude model specifies a useful linear relationship between these two variables.

$$P - \text{value} \cong 0.000002$$

b)  $\hat{\sigma}^2 = MS_E = \frac{SS_E}{n - 2} = \frac{22.123}{12} = 1.844$

- 6-14. a) Refer to ANOVA table of Exercise 6-4.  
1) The parameter of interest is the regressor variable coefficient,  $\beta_1$ .

- 2)  $H_0: \beta_1 = 0$
- 3)  $H_1: \beta_1 \neq 0$
- 4)  $\alpha = 0.01$
- 5) The test statistic is

$$f_0 = \frac{MS_R}{MS_E} = \frac{SS_R / 1}{SS_E / (n - 2)}$$

- 6) Reject  $H_0$  if  $f_0 > f_{\alpha, 1, 26}$  where  $f_{0.01, 1, 26} = 7.724$
- 7) Using the results of Exercise 6-4

$$f_0 = \frac{MS_R}{MS_E} = 31.1032$$

- 8) Since  $31.1032 > 7.724$  reject  $H_0$  and conclude the model is useful at  $\alpha = 0.01$ .  
P-value = 0.000007

b)  $\hat{\sigma}^2 = MS_E = 5.72585$

- c) 2)  $H_0: \beta_1 = 0$
- 3)  $H_1: \beta_1 \neq 0$
- 4)  $\alpha = 0.01$
- 5) The test statistic is

$$t_0 = \frac{\hat{\beta}_1}{se(\hat{\beta}_1)}$$

- 6) Reject  $H_0$  if  $t_0 < -t_{\alpha/2, n-2}$  where  $-t_{0.005, 26} = -2.78$  or  $t_0 > t_{0.005, 26} = 2.78$
- 7) Using the results from Exercise 6-4

$$t_0 = \frac{-0.0070251}{0.00125965} = -5.577$$

- 8) Since  $-5.577 < -2.78$  reject  $H_0$  and conclude the regressor is useful in the model at  $\alpha = 0.01$ .

6-16. Refer to ANOVA for Exercise 6-6

- a) 1) The parameter of interest is the regressor variable coefficient,  $\beta_1$ .
- 2)  $H_0: \beta_1 = 0$
- 3)  $H_1: \beta_1 \neq 0$
- 4)  $\alpha = 0.01$
- 5) The test statistic is

$$f_0 = \frac{MS_R}{MS_E} = \frac{SS_R / 1}{SS_E / (n - 2)}$$

- 6) Reject  $H_0$  if  $f_0 > f_{\alpha, 1, 22}$  where  $f_{0.01, 1, 22} = 10.049$
- 7) Using the results from Exercise 6-6

$$f_0 = \frac{280583.12 / 1}{37.746089 / 10} = 74334.4$$

- 8) Since  $74334.4 > 10.049$ , reject  $H_0$  and conclude the model is useful  $\alpha = 0.01$ .  
P-value < 0.000001

b)  $MSE = SS_E / (n - p) = \hat{\sigma}^2 = 3.77461$

- c) 1) The parameter of interest is the regressor variable coefficient,  $\beta_1$ .  
 2)  $H_0: \beta_1 = 10$   
 3)  $H_1: \beta_1 \neq 10$   
 4)  $\alpha = 0.01$   
 5) The test statistic is

$$t_0 = \frac{\hat{\beta}_1 - \beta_{1,0}}{se(\hat{\beta}_1)}$$

- 6) Reject  $H_0$  if  $t_0 < -t_{\alpha/2, n-2}$  where  $-t_{0.005, 10} = -3.17$  or  $t_0 > t_{0.005, 10} = 3.17$   
 7) Using the results from Exercise 6-6

$$t_0 = \frac{9.21 - 10}{0.0338} = -23.37$$

- 8) Since  $-23.37 < -3.17$  reject  $H_0$  and conclude the regressor is useful at  $\alpha = 0.01$ .

P-value = 0.

- 6-18. a)  $\beta_1: t_0 = 4.82$  P-value =  $2(4.08 \text{ E-}5) = 8.16 \text{ E-}5$   
 $\beta_2: t_0 = 8.21$  P-value =  $2(1.91 \text{ E-}8) = 3.82 \text{ E-}8$   
 $\beta_3: t_0 = 0.98$  P-value =  $2(0.1689) = 0.3378$

- b) 2)  $H_0: \beta_3 = 0$   
 3)  $H_1: \beta_3 \neq 0$   
 4)  $\alpha = 0.05$   
 5) Reject  $H_0$  if  $t_0 < -t_{\alpha/2, n-2}$  where  $-t_{0.025, 23} = -2.074$  or  $t_0 > t_{\alpha/2, n-2}$  where  $t_{0.025, 23} = 2.074$   
 6)  $t_0 = 0.98$   
 7) Since  $-2.074 < 0.98 < 2.074$  do not reject  $H_0$  and conclude that  $x_3$  is not useful as a regressor in the model at  $\alpha = 0.05$ .

6-20.

Analysis of Variance for the Full Regression

Source value	Sum of Squares	DF	Mean Square	F-Ratio	P-
Model	12161.6	2	6080.79	9.35303	
Error	1950.42	3	650.141		
Total (Corr.)	14112.0	5			

R-squared = 0.86179  
 25.4979

Std. error of est. =

R-squared (Adj. for d.f.) = 0.76965  
 2.56509

Durbin-Watson statistic =

Assume no interaction.

- a) 1) The parameters of interest are the regression coefficients,  $\beta_j$ .  
 2)  $H_0: \beta_1 = \beta_2 = 0$   
 3)  $H_1$ : at least one  $\beta_j \neq 0$   
 4)  $\alpha = 0.05$   
 5) The test statistic is

$$f_0 = \frac{SS_R / k}{SS_E / (n - p)}$$

- 6) Reject  $H_0$  if  $f_0 > f_{\alpha,2,3}$  where  $f_{0.05,2,3} = 9.55$   
 7) Using the results from the ANOVA Table above

$$f_0 = 9.35$$

If  $f_0$  is to be calculated by hand, use Equation (6-34).

- 8) Since  $9.35 < 9.55$  do not reject  $H_0$  and conclude the regressors are not significantly useful as regressors in the model at  $\alpha = 0.05$ .

$$P\text{-value} = 0.0514$$

b)

Model fitting results for: y

Independent variable sig.level	coefficient	std. error	t-value
CONSTANT 0.0183	350.994271	74.753074	4.6954
x1 0.3562	-1.271994	1.16914	-1.0880
x2 0.1841	-0.153904	0.08953	-1.7190

R-SQ. (ADJ.) = 0.7696 SE= 25.497858 MAE= 16.319125 DurbWat= 2.565  
 Previously: 0.0000 0.000000 0.000000  
 6 observations fitted, forecast(s) computed for 0 missing val. of dep. var.

$$H_0: \beta_1 = 0$$

$$H_0: \beta_2 = 0$$

$$H_1: \beta_1 \neq 0$$

$$H_1: \beta_2 \neq 0$$

$$t_0 = -1.09$$

$$t_0 = -1.72$$

$$t_{\alpha/2,3} = t_{.025,3} = 3.182$$

$$t_{\alpha/2,3} = t_{.025,3} = 3.182$$

Since  $-3.182 < -1.09 < 3.182$  for  $\beta_1$ , and  $-3.182 < -1.72 < 3.182$  for  $\beta_2$ , do not reject  $H_0$  for either regressor and

conclude that  $x_1$  and  $x_2$  are not significantly useful as regressors for this model at  $\alpha = 0.05$

If  $t_0$  is to be calculated by hand, use Equation (6-38).

6-22.

Analysis of Variance for the Full Regression

Source value	Sum of Squares	DF	Mean Square	F-Ratio	P-
Model .0000	30531.5	3	10177.2	840.546	
Error	193.725	16	12.1078		
Total (Corr.)	30725.2	19			

$$R\text{-squared} = 0.993695$$

$$\text{Std. error of est.} = 3.47963$$

$$R\text{-squared (Adj. for d.f.)} = 0.992513$$

$$\text{Durbin-Watson statistic} = 1.77758$$

- a) 1) The parameters of interest are the regression coefficients,  $\beta_j$ .

- 2)  $H_0: \beta_j = 0$  for all j
- 3)  $H_1: \beta_j \neq 0$  for at least one j
- 4)  $\alpha = 0.05$
- 5) The test statistic is

$$f_0 = \frac{SS_R / k}{SS_E / (n - p)}$$

- 6) Reject  $H_0$  if  $f_0 > f_{\alpha,3,16}$  where  $f_{0.05,3,16} = 3.24$
- 7) Using the results from the ANOVA table

$$f_0 = 840.55$$

If  $f_0$  is to be calculated by hand, use Equation (6-34).

8) Since  $840.55 > 3.24$  reject  $H_0$  and conclude the regressors are not significantly useful as regressors in the model at  $\alpha = 0.05$ .

b)  $\hat{\sigma}^2 = 12.1078$

c)

Model fitting results for: y

```

-----
--
Independent variable      coefficient  std. error  t-value
sig.level
-----
--
CONSTANT                 47.173999   49.581476   0.9514
0.3555
x1                       -9.735202   3.691625   -2.6371
0.0179
x2                        0.428287   0.223933   1.9126
0.0739
x3                       18.237455   1.311802   13.9026
0.0000
-----
--
R-SQ. (ADJ.) = 0.9925  SE=      3.479627  MAE=      2.511105  DurbWat=
1.778
Previously:   0.0000      0.000000      0.000000
0.000
20 observations fitted, forecast(s) computed for 0 missing val. of dep. var.

```

$\alpha = 0.05$	$t_{\alpha/2, n-p} = t_{0.025, 16} = 2.12$	
$H_0: \beta_1 = 0$	$\beta_2 = 0$	$\beta_3 = 0$
$H_1: \beta_1 \neq 0$	$\beta_2 \neq 0$	$\beta_3 \neq 0$
$t_0 = -2.637$	$t_0 = 1.91$	$t_0 = 13.90$
$-2.637 < -2.12$	$-2.12 < 1.91 < 2.12$	$13.9 > 2.12$
Reject $H_0$	Do not reject $H_0$	Reject $H_0$

$\beta_1$  : Reject  $H_0$  and conclude that  $x_1$  is a significant regressor in the model at  $\alpha = 0.05$ .

$\beta_2$  : Do not reject  $H_0$  and conclude that  $x_2$  is not a significant regressor in the model at  $\alpha = 0.05$ .

$\beta_3$  : Reject  $H_0$  and conclude that  $x_3$  is a significant regressor in the model at  $\alpha = 0.05$ .

## Chapter 7 (Problems 7.1-7.8)

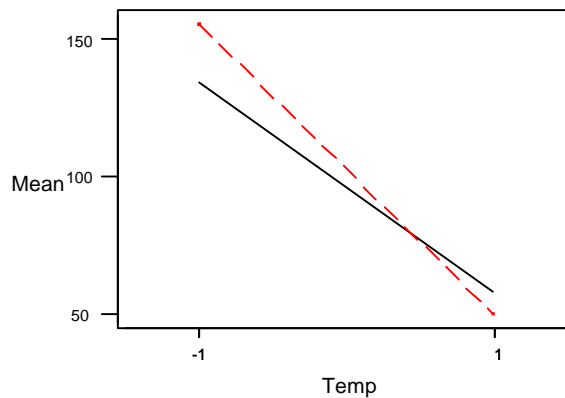
7-1.

a) Estimated Effects and Coefficients for Life

Term	Effect	Coef	StDev	Coef	T	P
Constant		99.38		7.711	12.89	0.000
Material	6.50	3.25		7.711	0.42	0.681
Temp	-91.75	-45.87		7.711	-5.95	0.000
Material*Temp	-14.50	-7.25		7.711	-0.94	0.366

b)

Interaction Plot for Life



The interaction plot does not indicate a strong interaction between temperature and material.

c) The t-ratios are given in the output shown in part a. The t-ratios indicate that temperature is significant, but material and the interaction material\*temperature are not at the  $\alpha = 0.05$  level.

d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.

Temperature:  $\text{s.e.}(\text{effect}) = 2(7.711) = 15.42$

Approximate 95% confidence interval on the the effect of Temperature:

$$6.5 \pm 2(15.42)$$

$$(-24.34, 37.34)$$

Material:  $\text{s.e.}(\text{effect}) = 2(7.711) = 15.42$

Approximate 95% confidence interval for the effect of Material:

$$-91.75 \pm 2(15.42)$$

$$(-122.59, -60.91)$$

Material\*Temperature:  $\text{s.e.}(\text{effect}) = 2(7.711) = 15.42$

Approximate 95% confidence interval for the effect of Material\*Temperature:

$$-14.50 \pm 2(15.42)$$

$$(-45.34, 16.34)$$

e)

The regression equation is

$$\text{Life} = 99.4 + 3.25 \text{ Material} - 45.9 \text{ Temp} - 7.25 \text{ Material*Temp}$$

Predictor	Coef	StDev	T	P
Constant	99.375	7.711	12.89	0.000
Material	3.250	7.711	0.42	0.681
Temp	-45.875	7.711	-5.95	0.000
Material*Temp	-7.250	7.711	-0.94	0.366

Based on the regression analysis, only temperature appears to be the significant factor. This result is equivalent to that obtained in part c.

The final regression analysis and model are

$$\text{Life} = 99.4 - 45.9 \text{ Temp}$$

Predictor	Coef	StDev	T	P
Constant	99.375	7.448	13.34	0.000
Temp	-45.875	7.448	-6.16	0.000

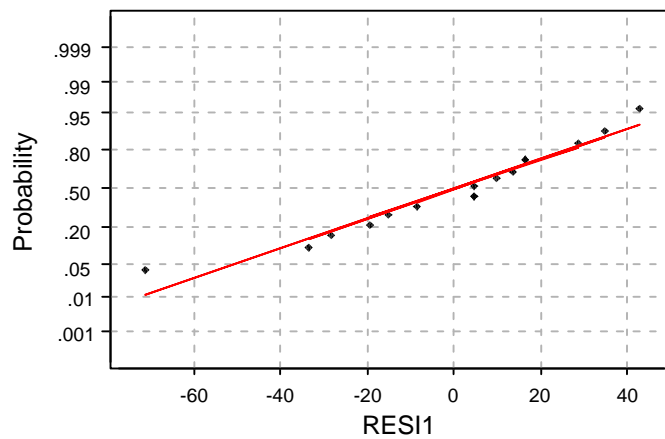
S = 29.79      R-Sq = 73.0%      R-Sq(adj) = 71.1%

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	1	33672	33672	37.94	0.000
Error	14	12426	888		
Total	15	46098			

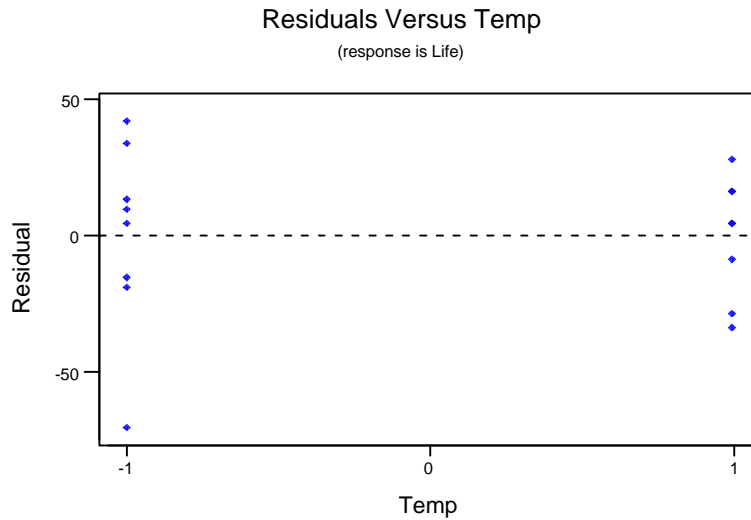
The analysis of variance indicates the final regression model is adequate for this set of data. This is evident by p-value  $\cong$  0.000.

### Normal Probability Plot



Average: -0.0000000  
StDev: 28.7814  
N: 16

Anderson-Darling Normality Test  
A-Squared: 0.324  
P-Value: 0.493

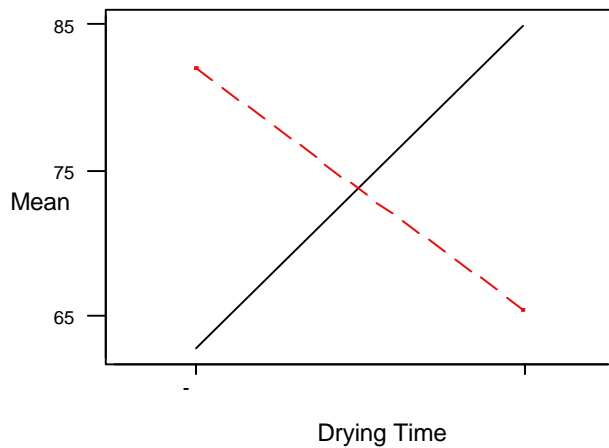


There does not appear to be any serious departure from normality shown in the normal probability plot of the residuals. The assumption of constant variance does not appear to be violated. The residuals appear to have the same spread for both levels of Temperature.

7-2. a) Estimated Effects and Coefficients for Surface

Term	Effect	Coef	StDev	Coef	T	P
Constant		73.750		3.955	18.65	0.000
Paint	-0.167	-0.083		3.955	-0.02	0.984
Drying	2.833	1.417		3.955	0.36	0.729
Paint*Drying	-19.500	-9.750		3.955	-2.47	0.039

b) Interaction Plot for Surface



The interaction plot indicates an interaction between drying time and paint type.

c) The t-ratios are given in the output shown in part a. The t-ratios indicate that the interaction of Paint type\*Drying Time is significant at the  $\alpha = 0.05$  level.

d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.

Paint Type:  $\text{s.e.}(\text{effect}) = 2(3.955) = 7.91$   
 Approximate 95% confidence interval on the the effect of Paint Type:

$-0.167 \pm 2(7.91)$   
 $(-15.987, 15.653)$

Drying Time:  $\text{s.e.}(\text{effect}) = 2(3.955) = 7.91$   
 Approximate 95% confidence interval for the effect of Drying Time:

$2.833 \pm 2(7.91)$   
 $(-12.987, 18.653)$

Paint Type\*Drying Time:  $\text{s.e.}(\text{effect}) = 2(3.955) = 7.91$   
 Approximate 95% confidence interval for the effect of Paint Type\*Drying Time:

$-19.50 \pm 2(7.91)$   
 $(-35.32, -3.68)$

e) The regression analysis and, in this case, the final model are

The regression equation is  
 Surface Finish = 73.8 - 0.08 Paint Type + 1.42 Drying Time  
 - 9.75 Paint Type\*Drying Time

Predictor	Coef	StDev	T	P
Constant	73.750	3.955	18.65	0.000
Paint Ty	-0.083	3.955	-0.02	0.984
Drying T	1.417	3.955	0.36	0.729
Paint*Drying	-9.750	3.955	-2.47	0.039

S = 13.70      R-Sq = 43.7%      R-Sq(adj) = 22.6%

the Based on the regression analysis, only the interaction appears to be significant. Since we have adopted procedure of using hierarchical models, then this result is equivalent to that obtained in part c.

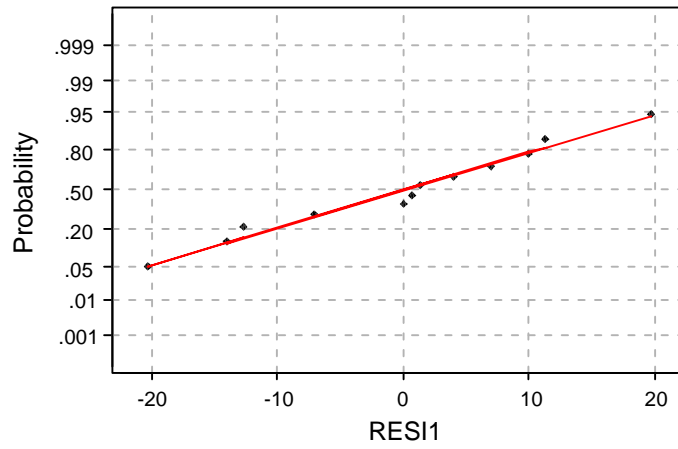
Analysis of Variance

Source	DF	SS	MS	F	P
Regression	3	1164.9	388.3	2.07	0.183
Error	8	1501.3	187.7		
Total	11	2666.2			

Source	DF	Seq SS
Paint Ty	1	0.1
Drying T	1	24.1
Paint Ty	1	1140.7

The analysis of variance may indicate the final regression model is inadequate for this set of data. The adequacy may be influenced by the inclusion of the insignificant main effects to maintain hierarchy.

### Normal Probability Plot

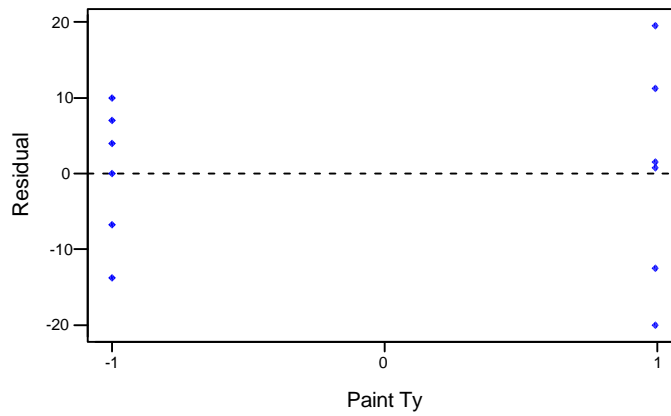


Average: -0.0000000  
 StDev: 11.6827  
 N: 12

Anderson-Darling Normality Test  
 A-Squared: 0.200  
 P-Value: 0.846

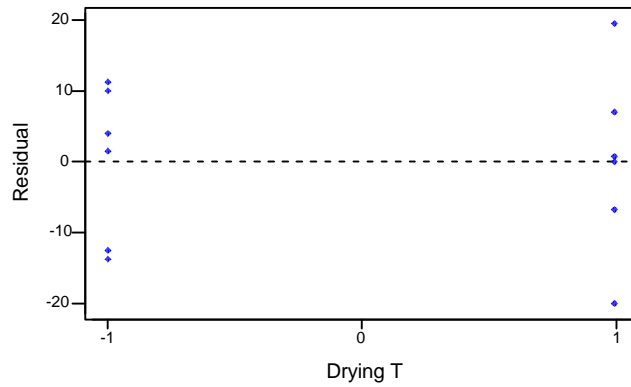
### Residuals Versus Paint Ty

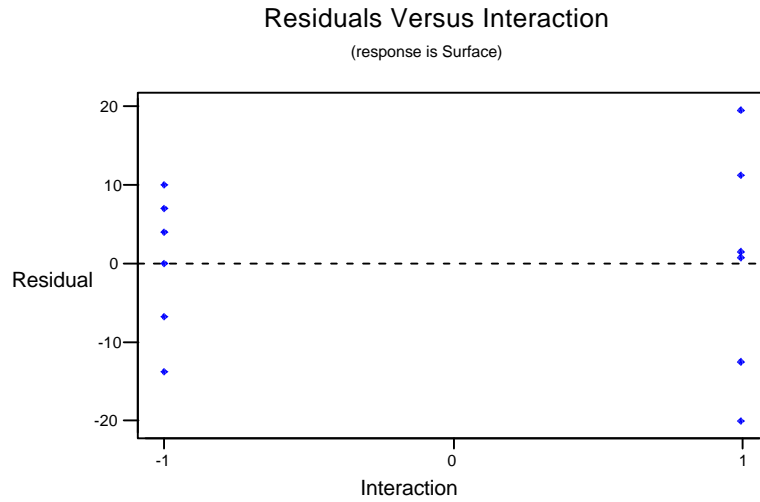
(response is Surface)



### Residuals Versus Drying T

(response is Surface)



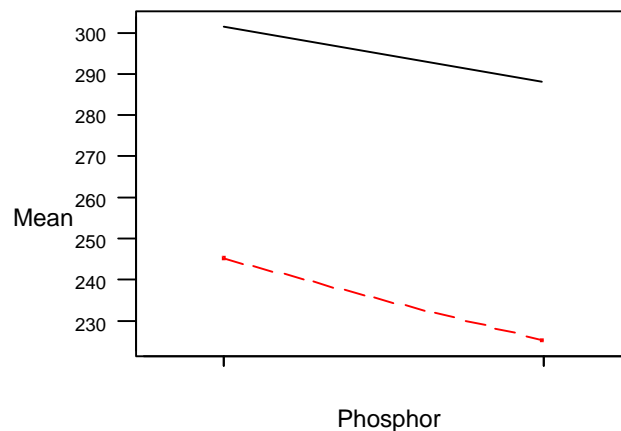


There does not appear to be any serious departure from normality shown in the normal probability plot of the residuals. The assumption of constant variance does not appear to be seriously violated. The residuals for the high level of the interaction appear to be slightly more spread out than those for the low level.

7-3. a) Estimated Effects and Coefficients for current

Term	Effect	Coef	StDev	Coef	T	P
Constant		265.00	2.357	112.43	0.000	
Glass	-60.00	-30.00	2.357	-12.73	0.000	
Phosphor	-16.67	-8.33	2.357	-3.54	0.008	
Glass*Phosphor	-3.33	-1.67	2.357	-0.71	0.500	

b) Interaction Plot for current



The interaction plot does not indicate any significant interaction between Glass and Phosphor type.

c) The t-ratios are given in the output shown in part a. The t-ratios indicate that both Glass type and Phosphor type are significant at the  $\alpha = 0.05$  level.

d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.

Glass Type:  $\text{s.e.}(\text{effect}) = 2(2.357) = 4.714$

Approximate 95% confidence interval on the the effect of Glass Type:

$-60.0 \pm 2(4.714)$   
 $(-69.43, -50.57)$

Phosphor Type:  $\text{s.e.}(\text{effect}) = 2(2.357) = 4.714$

Approximate 95% confidence interval for the effect of Phosphor Type:

$-16.67 \pm 2(4.714)$   
 $(-26.1, -7.242)$

Glass Type\*Phosphor Type:  $\text{s.e.}(\text{effect}) = 2(2.357) = 4.714$

Approximate 95% confidence interval for the effect of Glass Type\*Phosphor Type:

$-3.33 \pm 2(4.714)$   
 $(-12.76, -6.1)$

e)

The regression equation is

current = 265 - 30.0 Glass - 8.33 Phosphor - 1.67 Glass\*Phosphor

Predictor	Coef	StDev	T	P
Constant	265.000	2.357	112.43	0.000
Glass	-30.000	2.357	-12.73	0.000
Phosphor	-8.333	2.357	-3.54	0.008
Glass*Ph	-1.667	2.357	-0.71	0.500

Based on the regression analysis, both Glass type and Phosphor type appear to be the significant factors. This result is equivalent to that obtained in part c.

The regression analysis and final model are:

The regression equation is

current = 265 - 30.0 Glass - 8.33 Phosphor

Predictor	Coef	StDev	T	P
Constant	265.000	2.291	115.69	0.000
Glass	-30.000	2.291	-13.10	0.000
Phosphor	-8.333	2.291	-3.64	0.005

S = 7.935      R-Sq = 95.4%      R-Sq(adj) = 94.3%

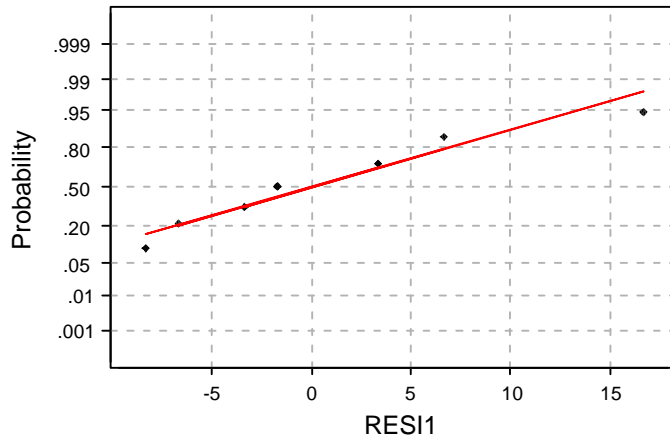
Analysis of Variance

Source	DF	SS	MS	F	P
Regression	2	11633.3	5816.7	92.38	0.000
Error	9	566.7	63.0		
Total	11	12200.0			

Source	DF	Seq SS
Glass	1	10800.0
Phosphor	1	833.3

The analysis of variance indicates the final regression model is adequate for this set of data. This is evident by p-value  $\cong 0.000$ .

### Normal Probability Plot

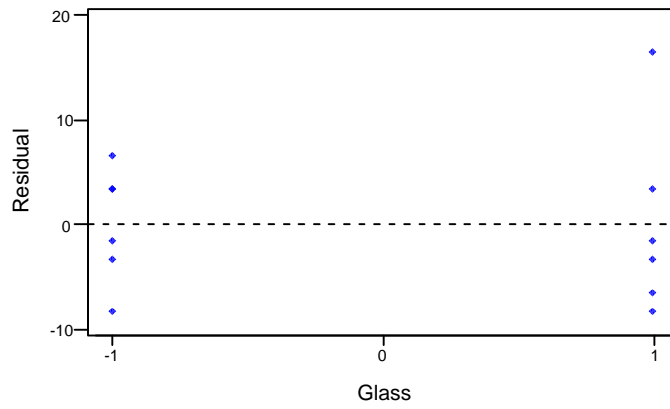


Average: 0  
 StDev: 7.17741  
 N: 12

Anderson-Darling Normality Test  
 A-Squared: 0.408  
 P-Value: 0.292

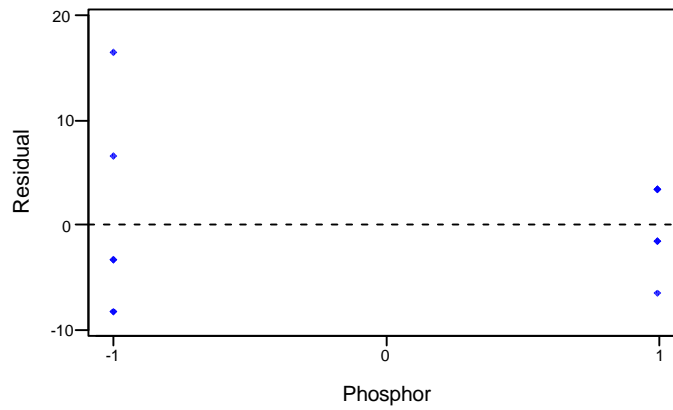
### Residuals Versus Glass

(response is current)



### Residuals Versus Phosphor

(response is current)



There does not appear to be any serious departure from normality shown in the normal probability plot of the residuals. As for constant variance the residuals appear to be more spread out for the low level of Phosphor, while they are more spread out for the high level of Glass.

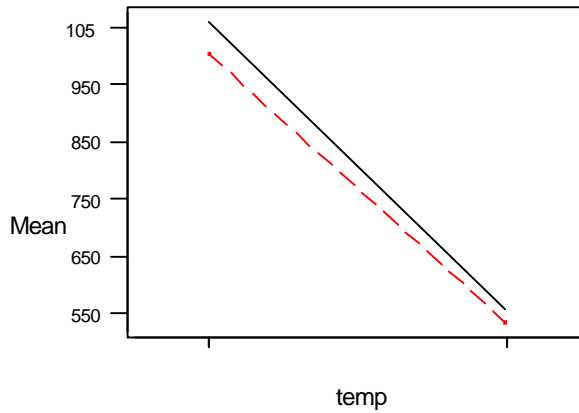
7-4.

a) Estimated Effects and Coefficients for density

Term	Effect	Coef	StDev	Coef	T	P
Constant		788.8		7.098	111.13	0.000
position	-39.5	-19.8		7.098	-2.78	0.024
temp	-490.5	-245.2		7.098	-34.55	0.000
position*temp	16.5	8.3		7.098	1.16	0.279

b)

Interaction Plot for density



The interaction plot does not indicate a significant interaction between temperature and position.

- c) The t-ratios are given in the output shown in part a. The t-ratios indicate that both Position and Temperature are significant at the  $\alpha = 0.05$  level.
- d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.
- Position:  $\text{s.e.}(\text{effect}) = 2(7.098) = 14.196$   
 Approximate 95% confidence interval on the the effect of Position:
- $$-39.5 \pm 2(14.196)$$
- $$(-67.89, -11.11)$$
- Temperature:  $\text{s.e.}(\text{effect}) = 2(7.098) = 14.196$   
 Approximate 95% confidence interval for the effect of Temperature:
- $$-490.5 \pm 2(14.196)$$
- $$(-518.89, -462.11)$$
- Position\*Temperature:  $\text{s.e.}(\text{effect}) = 2(7.098) = 14.196$   
 Approximate 95% confidence interval for the effect of Position\*Temperature:
- $$16.5 \pm 2(14.196)$$
- $$(-11.89, 44.89)$$

e)

The regression equation is  
 $\text{density} = 789 - 19.7 \text{ position} - 245 \text{ temp} + 8.25 \text{ Position*Temp}$

Predictor	Coef	StDev	T	P
Constant	788.750	7.098	111.13	0.000
position	-19.750	7.098	-2.78	0.024
temp	-245.250	7.098	-34.55	0.000
Position*Temp	8.250	7.098	1.16	0.279

Based on the regression analysis, both Position and Temperature appear to be the significant factors. This result is equivalent to that obtained in part c.

The regression analysis and final model are

The regression equation is  
 $\text{density} = 789 - 19.7 \text{ position} - 245 \text{ temp}$

Predictor	Coef	StDev	T	P
Constant	788.750	7.235	109.02	0.000
position	-19.750	7.235	-2.73	0.023
temp	-245.250	7.235	-33.90	0.000

S = 25.06      R-Sq = 99.2%      R-Sq(adj) = 99.1%

Analysis of Variance

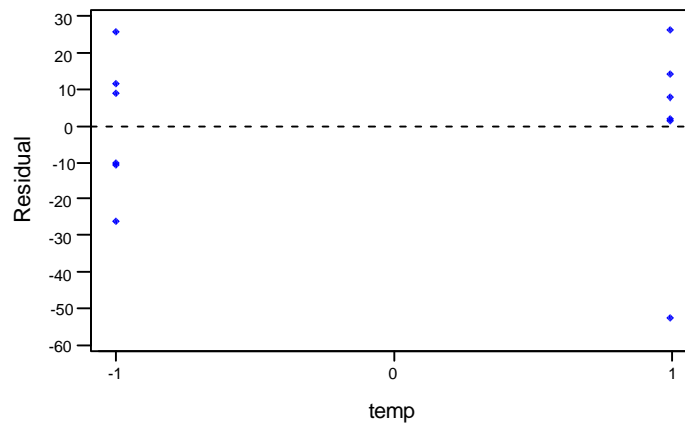
Source	DF	SS	MS	F	P
Regression	2	726451	363226	578.31	0.000
Error	9	5653	628		
Total	11	732104			

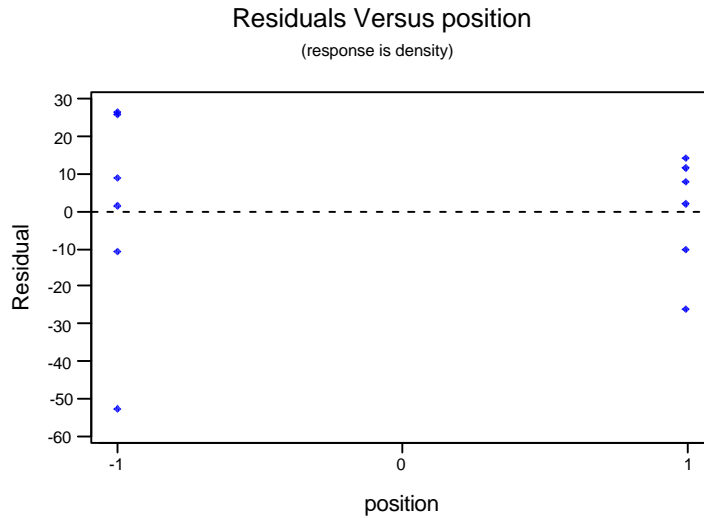
Source	DF	Seq SS
position	1	4681
temp	1	721771

The analysis of variance indicates the final regression model is adequate for this set of data. This is evident by p-value  $\cong 0.000$ .

Residuals Versus temp

(response is density)



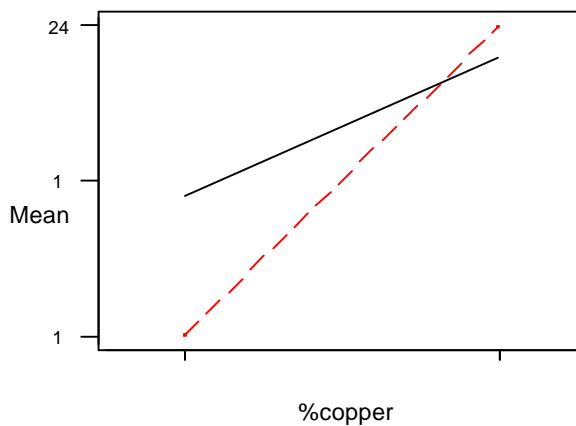


There does not appear to be any serious departure from normality shown in the normal probability plot of the residuals. The assumption of constant variance does not appear to be violated. The residuals appear to have approximately the same spread for both levels of Temperature and both levels of Position.

7-5. a) Estimated Effects and Coefficients for warping

Term	Effect	Coef	StDev	Coef	T	P
Constant		19.8750	0.7181	27.68	0.000	
temp	-1.7500	-0.8750	0.7181	-1.22	0.290	
%copper	7.2500	3.6250	0.7181	5.05	0.007	
temp*%copper	2.7500	1.3750	0.7181	1.91	0.128	

b) Interaction Plot for warping



The interaction plot indicates there may be a slightly significant interaction between %Copper and Temperature.

c) The t-ratios are given in the output shown in part a. The t-ratios indicate that only %Copper is significant at the  $\alpha = 0.05$  level.

d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.

Temperature:  $\text{s.e.}(\text{effect}) = 2(0.7181) = 1.436$   
 Approximate 95% confidence interval on the the effect of Temperature:

$-1.75 \pm 2(1.436)$   
 $(-4.622, 1.122)$

%Copper:  $\text{s.e.}(\text{effect}) = 2(0.7181) = 1.436$   
 Approximate 95% confidence interval for the effect of %Copper:

$7.25 \pm 2(1.436)$   
 $(4.378, 10.122)$

Temperature\*%Copper:  $\text{s.e.}(\text{effect}) = 2(0.7181) = 1.436$   
 Approximate 95% confidence interval for the effect of Temperature\*%Copper:

$2.75 \pm 2(1.436)$   
 $(-0.122, 5.622)$

e)

The regression equation is  
 $\text{warping} = 19.9 - 0.875 \text{ temp} + 3.63 \text{ \%copper} + 1.38 \text{ Temp*\%Copper}$

Predictor	Coef	StDev	T	P
Constant	19.8750	0.7181	27.68	0.000
temp	-0.8750	0.7181	-1.22	0.290
%copper	3.6250	0.7181	5.05	0.007
Temp*%Co	1.3750	0.7181	1.91	0.128

Based on the regression analysis, only %Copper appears to be the significant factor. This result is equivalent to that obtained in part c.

The regression analysis and final model are

The regression equation is  
 $\text{warping} = 19.9 + 3.62 \text{ \%copper}$

Predictor	Coef	StDev	T	P
Constant	19.8750	0.8868	22.41	0.000
%copper	3.6250	0.8868	4.09	0.006

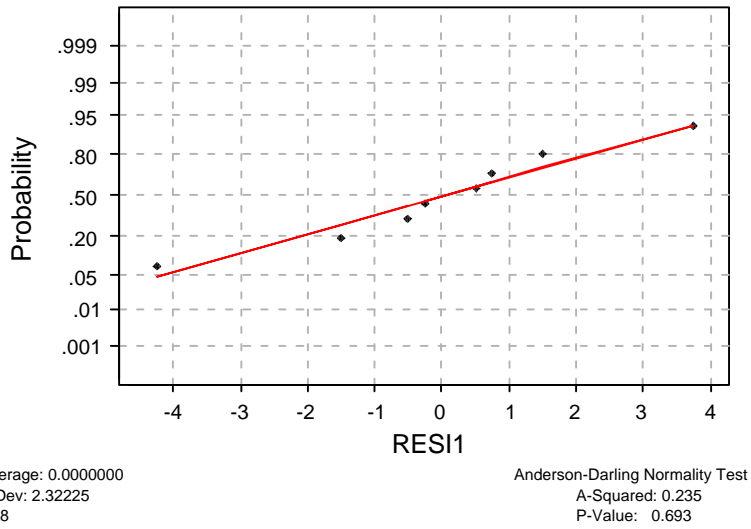
S = 2.508      R-Sq = 73.6%      R-Sq(adj) = 69.2%

Analysis of Variance

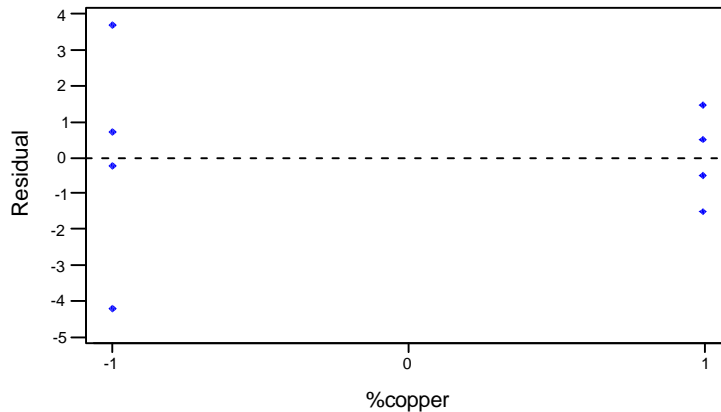
Source	DF	SS	MS	F	P
Regression	1	105.13	105.13	16.71	0.006
Error	6	37.75	6.29		
Total	7	142.88			

The analysis of variance indicates the final regression model is adequate for this set of data. This is evident by  $p\text{-value} \cong 0.006$ .

### Normal Probability Plot



### Residuals Versus %copper (response is warping)



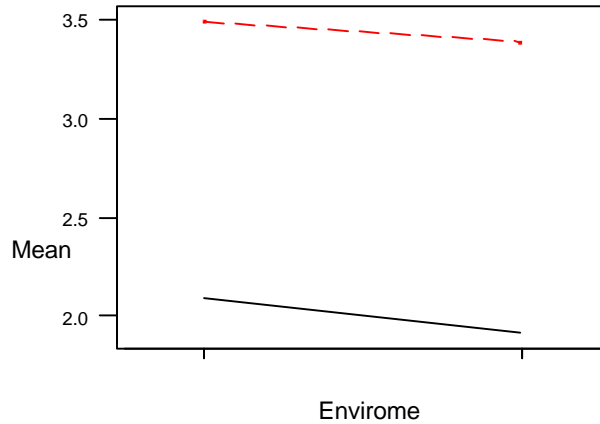
There does not appear to be any serious departure from normality shown in the normal probability plot of the residuals. The residuals for the low level of %Copper are more spread out than for the high level. The constant variance assumption may be a concern.

7-6. a) Estimated Effects and Coefficients for Fatigue

Term	Effect	Coef	StDev Coef	T	P
Constant		2.72187	0.07126	38.20	0.000
Frequenc	1.44125	0.72063	0.07126	10.11	0.000
Envirome	-0.14375	-0.07187	0.07126	-1.01	0.333
Frequenc*Envirome	0.03875	0.01937	0.07126	0.27	0.790

b)

### Interaction Plot for Fatigue



The interaction plot does not indicate a significant interaction between Environment and Frequency.

- c) The t-ratios are given in the output shown in part a. The t-ratios indicate that only Frequency is significant at the  $\alpha = 0.05$  level.
- d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.

Frequency:  $\text{s.e.}(\text{effect}) = 2(0.07126) = 0.1425$   
 Approximate 95% confidence interval on the the effect of Frequency:

$$1.44125 \pm 2(0.1425)$$

$$(1.299, 1.584)$$

Environment:  $\text{s.e.}(\text{effect}) = 2(0.07126) = 0.1425$   
 Approximate 95% confidence interval for the effect of Environment:

$$-0.14375 \pm 2(0.1425)$$

$$(-0.428, 0.142)$$

Frequency\*Environment:  $\text{s.e.}(\text{effect}) = 2(0.07126) = 0.1425$   
 Approximate 95% confidence interval for the effect of Frequency\*Environment:

$$0.03875 \pm 2(0.1425)$$

$$(-0.246, 0.324)$$

- e) The regression equation is  
 Fatigue = 2.72 + 0.721 Frequency - 0.0719 Environment + 0.0194  
 Freq\*Envir

Predictor	Coef	StDev	T	P
Constant	2.72187	0.07126	38.20	0.000
Frequenc	0.72063	0.07126	10.11	0.000
Envirome	-0.07187	0.07126	-1.01	0.333
Freq*Env	0.01938	0.07126	0.27	0.790

Based on the regression analysis, only Frequency appears to be the significant factor. This result is equivalent to that obtained in part c.

The regression analysis and final model are

The regression equation is  
 Fatigue = 2.72 + 0.721 Frequency

Predictor	Coef	StDev	T	P
Constant	2.72187	0.06891	39.50	0.000
Frequenc	0.72063	0.06891	10.46	0.000

S = 0.2756      R-Sq = 88.7%      R-Sq(adj) = 87.8%

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	1	8.3088	8.3088	109.36	0.000
Error	14	1.0636	0.0760		
Total	15	9.3724			

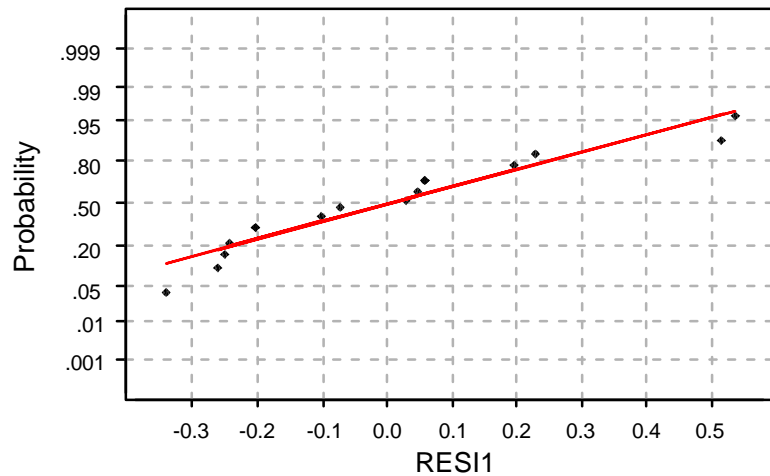
Unusual Observations

Obs	Frequenc	Fatigue	Fit	StDev Fit	Residual	St Resid
10	1.00	3.9600	3.4425	0.0975	0.5175	2.01R
12	1.00	3.9800	3.4425	0.0975	0.5375	2.08R

R denotes an observation with a large standardized residual

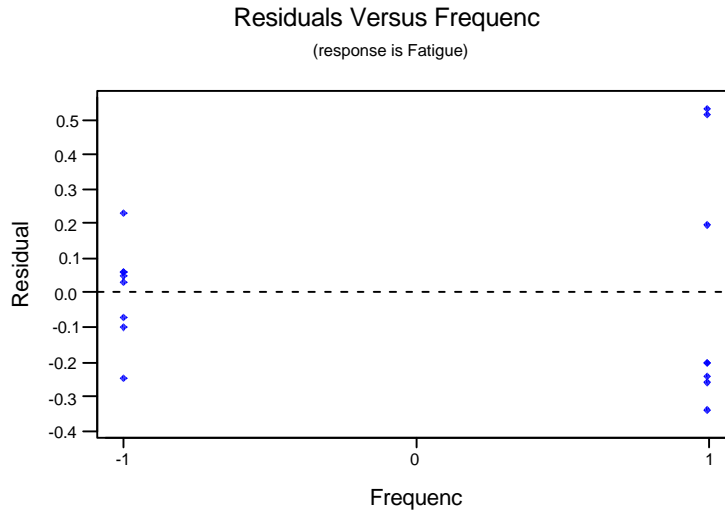
The analysis of variance indicates the final regression model is adequate for this set of data. This is evident by p-value  $\cong$  0.000.

### Normal Probability Plot



Average: 0.000000  
 StDev: 0.266288  
 N: 16

Anderson-Darling Normality Test  
 A-Squared: 0.522  
 P-Value: 0.156



There does not appear to be any serious departure from normality shown in the normal probability plot of the residuals. The residuals for the high level of Frequency are more spread out than for the low level. The constant variance assumption may be a concern.

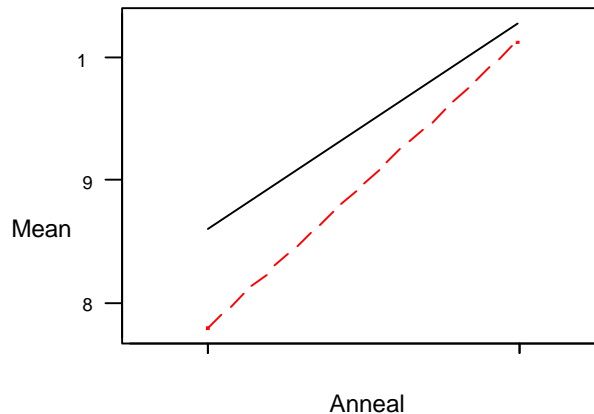
7-7.

a) Estimated Effects and Coefficients for Current

Term	Effect	Coef	StDev Coef	T	P
Constant		9.2050	0.07622	120.77	0.000
Polysili	-0.4850	-0.2425	0.07622	-3.18	0.033
Anneal	2.0300	1.0150	0.07622	13.32	0.000
Polysili*Anneal	0.3350	0.1675	0.07622	2.20	0.093

b)

Interaction Plot for Current



The interaction plot does not indicate a significant interaction between Polysilicon Doping and Anneal.

c) The t-ratios are given in the output shown in part a. The t-ratios indicate that both Polysilicon doping and Anneal are significant at the  $\alpha = 0.05$  level.

d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.

Polysilicon Doping:  $s.e.(effect) = 2(0.07622) = 0.1524$

Approximate 95% confidence interval on the the effect of Polysilicon Doping:

$-0.485 \pm 2(0.1524)$   
 $(-0.7898, -0.1802)$

Anneal:  $s.e.(effect) = 2(0.07622) = 0.1524$

Approximate 95% confidence interval for the effect of Anneal:

$2.03 \pm 2(0.1524)$   
 $(1.725, 2.34)$

Polysilicon doping\*Anneal:  $s.e.(effect) = 2(0.07622) = 0.1524$

Approximate 95% confidence interval for the effect of Polysilicon doping\*Anneal:

$0.335 \pm 2(0.1524)$   
 $(0.0302, 0.6398)$

e)

The regression equation is

Current = 9.21 - 0.242 Polysilicon + 1.02 Anneal + 0.167 Poly\*Anneal

Predictor	Coef	StDev	T	P
Constant	9.20500	0.07622	120.77	0.000
Polysili	-0.24250	0.07622	-3.18	0.033
Anneal	1.01500	0.07622	13.32	0.000
Poly*Ann	0.16750	0.07622	2.20	0.093

Based on the regression analysis, both Polysilicon and Anneal appear to be the significant factors. This result is equivalent to that obtained in part c.

The regression analysis and final model are

The regression equation is

Current = 9.21 - 0.242 Polysilicon + 1.02 Anneal

Predictor	Coef	StDev	T	P
Constant	9.2050	0.1013	90.88	0.000
Polysili	-0.2425	0.1013	-2.39	0.062
Anneal	1.0150	0.1013	10.02	0.000

S = 0.2865      R-Sq = 95.5%      R-Sq(adj) = 93.7%

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	2	8.7123	4.3561	53.08	0.000
Error	5	0.4103	0.0821		
Total	7	9.1226			

Source	DF	Seq SS
Polysili	1	0.4704
Anneal	1	8.2418

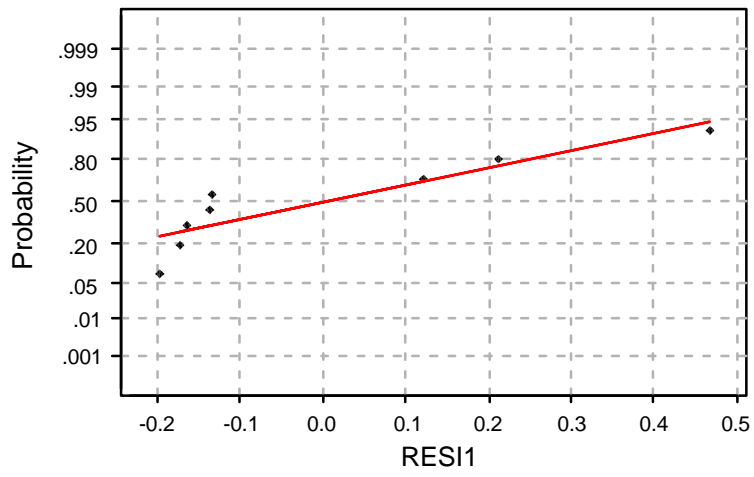
Unusual Observations

Obs	Polysili	Current	Fit	StDev Fit	Residual	St Resid
5	-1.00	8.900	8.432	0.175	0.468	2.06R

R denotes an observation with a large standardized residual

The analysis of variance indicates the final regression model is adequate for this set of data. This is evident by p-value  $\cong 0.000$ .

### Normal Probability Plot

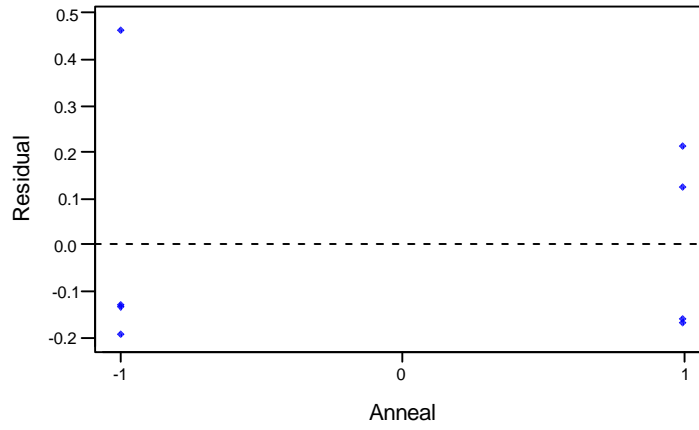


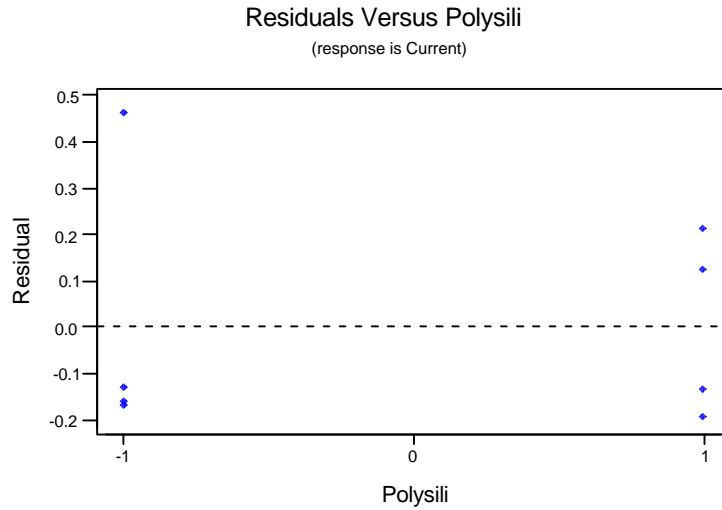
Average: 0  
StDev: 0.242119  
N: 8

Anderson-Darling Normality Test  
A-Squared: 0.747  
P-Value: 0.030

### Residuals Versus Anneal

(response is Current)





There does not appear to be any serious departure from normality shown in the normal probability plot of the residuals. The residuals for the high level of Anneal and for Polysilicon are more spread out than for the low levels of each. The constant variance assumption may be a concern.

7-8.

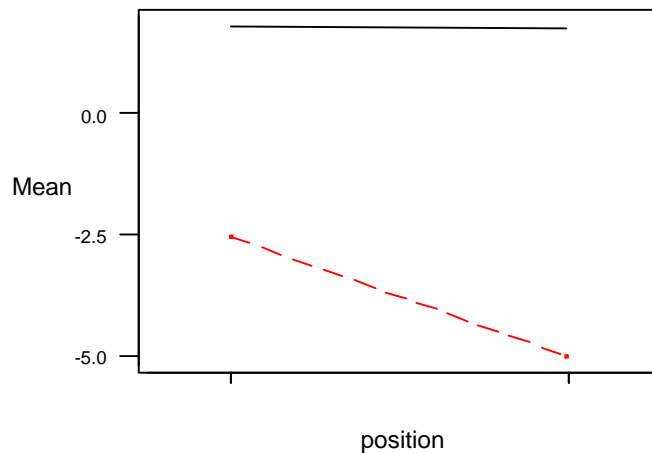
a)

Estimated Effects and Coefficients for charge

Term	Effect	Coef	StDev	Coef	T	P
Constant		-1.000	0.4462		-2.24	0.055
method	-5.593	-2.797	0.4462		-6.27	0.000
position	-1.280	-0.640	0.4462		-1.43	0.189
method*position	-1.220	-0.610	0.4462		-1.37	0.209

b)

Interaction Plot for charge



The interaction plot does not indicate a significant interaction between Method and Position.

c) The t-ratios are given in the output shown in part a. The t-ratios indicate that only Method is significant at the  $\alpha = 0.05$  level.

d) The 95% confidence intervals are given by effect estimate  $\pm 2(\text{s.e.}(\text{effect}))$  where  $\text{s.e.}(\text{effect}) = 2[\text{s.e.}(\text{coefficient})]$ . The  $\text{s.e.}(\text{coefficient})$  is given in the Minitab output of part a.

Method:  $\text{s.e.}(\text{effect}) = 2(0.4462) = 0.8924$

Approximate 95% confidence interval on the the effect of Method:

$-5.593 \pm 2(0.8924)$   
 $(-7.38, -0.3.81)$

Position:  $\text{s.e.}(\text{effect}) = 2(0.4462) = 0.8924$

Approximate 95% confidence interval for the effect of Position:

$-1.28 \pm 2(0.8924)$   
 $(-3.065, 0.505)$

Method\*Position:  $\text{s.e.}(\text{effect}) = 2(0.4462) = 0.8924$

Approximate 95% confidence interval for the effect of Method\*Position:

$-1.22 \pm 2(0.8924)$   
 $(-3.005, 0.565)$

e)

The regression equation is

charge = - 1.00 - 2.80 method - 0.640 position - 0.610 meth\*pos

Predictor	Coef	StDev	T	P
Constant	-1.0000	0.4462	-2.24	0.055
method	-2.7967	0.4462	-6.27	0.000
position	-0.6400	0.4462	-1.43	0.189
meth*pos	-0.6100	0.4462	-1.37	0.209

Based on the regression analysis, only Method appears to be the significant factor. This result is equivalent to that obtained in part c.

The regression analysis and final model are

The regression equation is

charge = - 1.00 - 2.80 method

Predictor	Coef	StDev	T	P
Constant	-1.0000	0.4873	-2.05	0.067
method	-2.7967	0.4873	-5.74	0.000

S = 1.688          R-Sq = 76.7%          R-Sq(adj) = 74.4%

Analysis of Variance

Source	DF	SS	MS	F	P
Regression	1	93.856	93.856	32.94	0.000
Error	10	28.490	2.849		
Total	11	122.347			

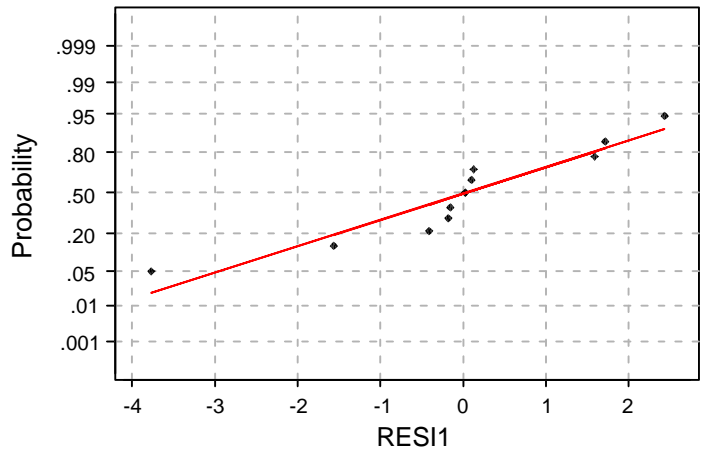
Unusual Observations

Obs	method	charge	Fit	StDev Fit	Residual	St Resid
4	1.00	-7.580	-3.797	0.689	-3.783	-2.46R

R denotes an observation with a large standardized residual

The analysis of variance indicates the final regression model is adequate for this set of data. This is evident by P-value  $\cong 0.000$ .

### Normal Probability Plot

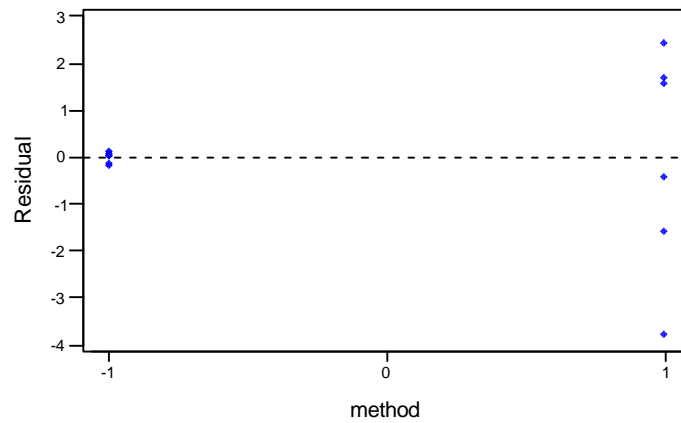


Average: 0.0000000  
StDev: 1.60936  
N: 12

Anderson-Darling Normality Test  
A-Squared: 0.667  
P-Value: 0.061

### Residuals Versus method

(response is charge)



The variance of the residuals for the high level of method are more spread out than for the low level. The constant variance assumption may be a concern.